

Decision Report

Application for Works Approval

Part V Division 3 of the Environmental Protection Act 1986

Works Approval Number W6626/2021/1 Applicant Northern Star (Carosue Dam) Pty Ltd ACN 116 649 122 File number DER2021/000666 **Premises** Carosue Dam Minesite Mining Tenements M28/269, M31/220 and M31/295 **MENZIES WA 6436** As defined by the premises map attached to the issued works approval Date of report 15 June 2022 Decision Works approval granted

Samara Rogers A/MANAGER, RESOURCE INDUSTRIES REGULATORY SERVICES

an officer delegated under section 20 of the Environmental Protection Act 1986 (WA)

Table of Contents

1.	Decision summary1						
2.	Scope	e of as	sessment1				
	2.1	Regula	atory framework1				
	2.2	Application summary and overview of premises1					
	2.3	Propos	ed works2				
	2.4	EPBC	Act1				
3.	Risk a	assess	ment1				
	3.1	Source	e-pathways and receptors1				
		3.1.1	Emissions and controls1				
		3.1.2	Receptors				
	3.2	Risk ra	atings2				
	3.3	Detaile	ed risk assessment for seepage from Carosue Dam TSF6				
		3.3.1	Background				
		3.3.2	Water balance				
		3.3.3	Current TSF seepage management9				
		3.3.4	Estimated seepage from proposed construction of Cell 4 and Cell 1-311				
		3.3.5	Risk rating of seepage12				
4.	Concl	usion					
Refe	rences	s					
Арре	endix 1	1: Desi	ign and construction of Cell 1-3 and Cell 415				
1.	Cell 1	-3 Des	ign15				
	1.1	Stage	4 of Cell 3				
	1.2	-	316				
2.	Cell 4	Desig	n19				
3.			rangement of TSF26				
App			lication validation summary27				
Table	e 1: Sun	nmary o	of TSF storage characteristics1				
		•	applicant controls1				
			uman and environmental receptors and distance from prescribed activity.3				
			sment of potential emissions and discharges from the premises during				

construction and operation	
Table 5: TSF annual water balance summary	8
Table 6: Consultation	13

Figure 1: Tailings storage plan (Cells 1-3 and 4) with forecast tailings production (FY22 to FY33)
Figure 2: Distance to sensitive receptors using 1 km buffer1
Figure 3: Water balance for the current TSF and associated processing infrastructure (unit = kL/month)7
Figure 4: Depth to water contour around TSF and Whirling Dervish – February to August 10
Figure 5: Estimated depth to groundwater after 10 years without recovery bores11
Figure 6: Estimated depth to groundwater after 10 years with recovery bores12
Figure 7: Current TSF cells. Cell 1-2 and Cell 315
Figure 8: Embankment design for Cell 3, Stage 416
Figure 9: Cell 3, Stage 416
Figure 10: Cell 1-3 design
Figure 11: Cell 4 design
Figure 12: Perimeter wall design with toe drain and cut off trench details21
Figure 13: Decant structure and decant causeway22
Figure 14: Underdrainage23
Figure 15: Return water pond to capture underdrainage24
Figure 16: Monitoring bores and piezometers25

1. Decision summary

This decision report documents the assessment of potential risks to the environment and public health from emissions and discharges during the construction and operation of the premises. As a result of this assessment, works approval W6626/2021/1 has been granted.

2. Scope of assessment

2.1 Regulatory framework

In completing the assessment documented in this decision report, the Department of Water and Environmental Regulation (the department; DWER) has considered and given due regard to its regulatory framework and relevant policy documents which are available at https://dwer.wa.gov.au/regulatory-documents.

2.2 Application summary and overview of premises

On 19 November 2021, the applicant submitted an application for a works approval to the department under section 54 of the *Environmental Protection Act 1986* (EP Act).

The application is to undertake construction works relating to Life of Mine tailings management at the premises. The premises is approximately 120 km north-east of the City of Kalgoorlie-Boulder.

The premises relates to the category 5 and assessed design capacity under Schedule 1 of the *Environmental Protection Regulations 1987* (EP Regulations) which are defined in works approval W6626/2021/1. The infrastructure and equipment relating to the premises category and any associated activities which the department has considered in line with *Guideline: Risk Assessments* (DWER 2020) are outlined in works approval W6626/2021/1.

Background

The cells currently in use for tailings storage were constructed in 2000(Cell 1), 2001 (Cell 2) and 2014 (Cell 3). Cells 1 and 2 were constructed with partial underdrainage and Cell 3 with underdrainage under the decant pond area. Cells 1 and 2 were merged as one cell in 2019 at Stage 7 of both cells design. The construction method for all three cells was that of upstream lifts after the initial downstream embankment was constructed.

Operation of the tailings storage facility is authorised under licence L7465/1999/9. This licence allows for discharge of tailings to the tailings storage facility up to Stage 3 of Cell 3 and Stage 7 of Cell 1-2. Cell 3 Stage 3 was expected to reach capacity during February 2022 at the time of application for this works approval (W6626/2021/1) and the Stage 8 construction of Cell 1-2 was expected to be completed in time for discharge to cease into Cell 3 Stage 3.

Stage 8 of Cell 1-2 has been constructed under works approval W6568/2021/1. Discharge into Cell 1-2 has commenced under the time limited operations conditions of W6568/2021/1.

The TSF, when constructed to the final design crest elevation, will provide approximately 30.3Mm3 of storage. This will provide an equivalent total storage capacity of approximately 44 Mt or more than 10 years' storage life, based on a projected tailings production rate of 4.1 Mtpa and an adopted tailings dry density of 1.45 t/m³. The current throughput under the premise licence L7465/1999/9 is 4Mtpa. Northern Star intends on increasing the permissible throughput of the CDO Processing Plant to 5Mt per annum during the current LOM TSF licence amendment.

2.3 **Proposed works**

The stages of the works assessed under this application are:

- Stage 1. Stage 4 of existing Cell 3 will be raised to an embankment crest level of RL 381 m, Figure 3;
- Stage 2. The new Cell 4, will be developed as a paddock-type facility to the west of existing Cell 3. A perimeter embankment to enclose an internal impoundment surface area of approximately 120 ha at starter embankment crest elevation of RL 375.5 m will be constructed, Figure 4;
- Stage 3. Merging of Cells 1-2 and Cell 3 to form a Supercell 1-3 at crest level of RL 383 m, Figure 10;
- Stage 4. A further 4 stages of upstream raised embankment will be constructed at Cell 4 with a final embankment crest elevation of RL 383.5 m (Cell 4 Stage 1 to Stage 4); and
- Stage 5. A further 3 stages of upstream raised embankment will be construction at Supercell 1-3 with final embankment crest elevation of RL 389 m (Supercell 1-3 Stage 2 to Stage 4).

Construction of Stages 1 -3 above will be approved under this works approval. They entail the establishment of the new arrangement for the tailings storage facility. The completion of Stage 3 of this works approval is expected to be completed by 2027 as per the timeline in Figure 1.

Stages 4 and 5 relate to the construction of ongoing lifts to the TSF facility the approval of which may be managed via licence amendments. These stages are not expected to be required until 2029. Specific requirements for each lift will be included in the corresponding Final Design Report which will be provided to DWER prior to commencement of each raise.

Figure 1 shows the projected production rate of tailings over the financial year against the planned stages of deposition for each TSF cell. Construction of each TSF cell stage occurs prior to the deposition period shown.

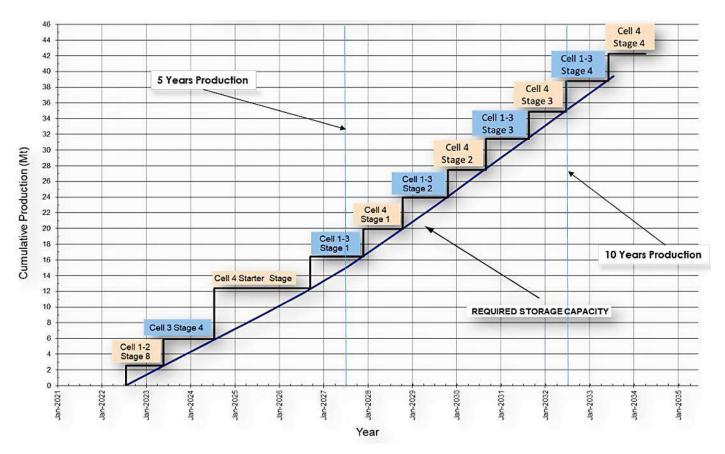


Figure 1: Tailings storage plan (Cells 1-3 and 4) with forecast tailings production (FY22 to FY33)

Table 1 shows the storage characteristics of each stage of the tailings storage development and an estimated time frame for each stage.

Construction details and design diagrams of Stages 1 - 3 of this works approval are provided in Appendix 1.

Stages proposed in Works approval application	TSF cell stage	Height of rise (m)	Embankment crest RL (m)	Storage area (ha)	Storage volume (Mm ³)	Cumulative storage volume (Mm ³)	Cumulative storage capacity (Mt)	Cumulative storage life (years)	Rate of rise (m/year)
1 ¹	Cell 3 Stage 4	3.5	381	72.0	2.37	5.33	5.56	1.99	3.04
2 ¹	Cell 4 starter embankment		375.5	120.7	4.44	9.77	12.40	4.16	1.84
31	Cell 1-3 Stage 1 (merging of Cell 1-2 with Cell 3)		383	137.9	2.77	12.54	16.42	5.35	1.68
4 and 5. ²	Cell 4 Stage 1	2	377.5	121.4	2.42	14.96	19.94	6.24	2.25
	Cell 1-3 Stage 2	2	385	135.3	2.76	17.72	23.96	7.26	1.97
	Cell 4 Stage 2	2	379.5	119.1	2.42	20.14	27.47	8.12	2.33
	Cell 1-3 Stage 3	2	387	132.7	2.72	22.86	31.42	9.08	2.07
	Cell 4 Stage 3	2	381.5	118.1	2.39	25.25	34.90	9.93	2.36
	Cell 1-3 Stage 4	2	389	130.2	2.66	27.91	38.77	10.88	2.12
	Cell 4 Stage 4	2	383.5	117.1	2.37	30.28	42.22	11.72	2.37

Table 1: Summary of TSF storage characteristics

1. Stages 1, 2 and 3 to be approved under this works approval.

2. Ongoing lifts to be managed through licence amendments

2.4 EPBC Act

The expansion of the TSF by the construction of Cell 4 was referred under the EPBC Act, managed by the Federal Department of Agriculture, Water and the Environment (DAWE), in relation to potential threat to malleefowl (*Leipoa ocellata*). The clearing of vegetation for the Cell 4 footprint will cause the destruction of malleefowl mounds. The decision from this referral was that; the proposed action is a controlled action and will require assessment and approval under the EPBC Act before it can proceed.

The Malleefowl Assessment (EPBC 2021-9026) under the EPBC Act is yet to be completed. This approval is managed DAWE in parallel to this Works Approval. No ground disturbance will commence until approval is granted by DAWE.

3. Risk assessment

The department assesses the risks of emissions from prescribed premises and identifies the potential source, pathway and impact to receptors in accordance with the *Guideline: Risk Assessments* (DWER 2020).

To establish a risk event there must be an emission, a receptor which may be exposed to that emission through an identified actual or likely pathway, and a potential adverse effect to the receptor from exposure to that emission.

3.1 Source-pathways and receptors

3.1.1 Emissions and controls

The key emissions and associated actual or likely pathway during premises construction and operation which have been considered in this decision report are detailed in Table 2 below. Table 2 also details the control measures the applicant has proposed to assist in controlling these emissions, where necessary.

Table 2:	Proposed	l applicant	controls
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Emission	Sources	Potential pathways	Proposed controls				
Construction							
Dust	Material handling,	Air / windborne pathway	Dust suppression using saline water sprays and water carts.				
	vehicle movements, earthworks etc.		Cessation of a particular operation or an amendment to an operational procedure when dust cannot be controlled.				
			Small, localised dust suppression, including mist spray.				
Commissior	ning and Operation	1					
Tailings	Leaks and spills	Direct contact	All pipelines will be:				
	from pipeline	with ground and vegetation.	 double skinned PE100 and will be constructed and installed in accordance 				
		Ground contamination causing	with AS4130 and AS413, and the Plastics Industry Pipe Association of Australia Limited (PIPA) Guideline POP003.				
		contamination of	contained within bunded open trenches				

Emission Sources Potential pathways			Proposed controls			
		stormwater.	sufficient in capacity to contain leaks and spillages between routine inspections.			
			 inspected twice daily as per DWER licence conditions. 			
			 fitted with automatic leak detection and shut off systems to minimise discharge and allow for maintenance and recovery of materials. The Citect processing plant control system monitors pressure in pipelines and water levels in tanks and dams. Upon an immediate drop in pressure within a pipeline or a dam is reaching capacity, mill control operators are alarmed and immediately shut down the plant to stop flow of material 			
	Overtopping of facility	Direct contact with ground and vegetation. Ground	The embankments of the TSF are constructed to provide a minimum 0.5 m total freeboard (including an allowance for a 1% AEP 72 hour rain event) above the normal operating pond.			
		contamination causing contamination of stormwater.	Licence (7465/1999/9) condition 4 requires a total freeboard of 500mm and an operational freeboard is required by licence for all containment cells, dams, ponds and turkeys nests on the premises.			
			12 hour inspections.			
	Dust from dry tailings	Air / windborne pathway.	Due to the short timeframe between lifts, dusting of tailings is not expected to occur as the material will retain moisture from operation of the cell.			
Leachate	Seepage through base of TSF.	Groundwater contamination Groundwater mounding	The supernatant pond size, when present, will be minimised as far as possible during operation of the facility, which will in turn reduce the risk of phreatic surface daylighting at the downstream face of the embankment and minimise outgoing seepage through the base of the TSF and its embankments.			
			Underdrainage installed across base of TSF with a return water pond to capture it for pumping back to the process circuit.			
			Monitoring bores installed around the TSF cells with a site trigger of 6mbgl for actions to be taken and a licence limit of 4mbgl.			
Decant return	Leaks and spills	Direct contact	All pipelines will be:			
water	from pipeline with ground and vegetation. Ground contamination causing contamination of		 double skinned PE100 and will be constructed and installed in accordance with AS4130 and AS413, and the Plastics Industry Pipe Association of Australia Limited (PIPA) Guideline POP003. 			

Emission	ission Sources Potential pathways		Proposed controls
		stormwater.	 contained within bunded open trenches sufficient in capacity to contain leaks and spillages between routine inspections.
			 inspected twice daily as per DWER licence conditions.
			 fitted with automatic leak detection and shut off systems to minimise discharge and allow for maintenance and recovery of materials. The Citect processing plant control system monitors pressure in pipelines and water levels in tanks and dams. Upon an immediate drop in pressure within a pipeline or a dam is reaching capacity, pumps are automatically shut off and mill control operators are alarmed to immediately shut down the plant to stop flow of material
	Overtopping of process water dam	Direct contact with ground and vegetation. Ground contamination causing contamination of stormwater	Licence (7465/1999/9) condition 4 requires a total freeboard of 500mm and an operational freeboard is required by licence for all containment cells, dams, ponds and turkeys nests on the premises.

3.1.2 Receptors

In accordance with the *Guideline: Risk Assessment* (DWER 2020), the Delegated Officer has excluded the applicant's employees, visitors, and contractors from its assessment. Protection of these parties often involves different exposure risks and prevention strategies, and is provided for under other state legislation.

Table 33 and Figure 2 below provides a summary of potential human and environmental receptors that may be impacted as a result of activities upon or emission and discharges from the prescribed premises (*Guideline: Environmental Siting* (DWER 2020)).

Table 3: Sensitive human and environmental receptors and distance from prescribed	
activity	

Human receptors	Distance from activity / prescribed premises		
City of Kalgoorlie-Boulder	Approximately 120km south-west of the Premises.		
Pinjin Station	37km from the tailings storage facility		
Environmental receptors	Distance from activity / prescribed premises		
Lake Rebecca – (salt lake)	7-8 km north east (down hydraulic gradient) of the TSF		
Underlying groundwater (non-potable purposes)	Within the Goldfields Groundwater Area (RIWI Act 1914 designated area). The groundwater level prior to operations was approximately 20 metres below ground level (mbgl). It has been locally modified by the TSF		

Works approval: W6626/2021/1

	operations and dewatering of pits.
	Groundwater is hypersaline with total dissolved solids (TDS) content being approximately 40,000mg/L.
	Pastoral bores
	- Relief Hill Well, ~5.5km east of the process plant and TSF
	- Y4 bore – ~10km north of the process plant and TSF
	Groundwater in the TSF area has been modified by the construction and operation of the existing TSF as well as dewatering and mining of the Whirling Dervish open pit. Groundwater mounding is evident in the TSF area with water levels rising in the north and west. In contrast, dewatering at Whirling Dervish has created a groundwater sink with water levels in the South east corner (MB1D) falling 26m. Water levels around the existing TSF vary depending on which cell is in operation. The standing water level (SWL) is highest on the north-eastern margin of the facility at MB6s (7.58mbgl in December 2021) and MB5 (8.37mbgl across the 2021 monitoring period).
Surface water	Catchments to the southwest and h of the TSF is currently diverted from the TSF Cell 3. Cell 4 will extend further into these catchment areas.
Native vegetation.	Acacia aneura (mulga) low woodlands associated with red loams over siliceous hard pan to the north and low woodlands of mixed mulga and Casuarina pauper (black oak) and Eucalyptus sp. on alkaline and calcareous soils to the south. Spinifex hummock grassland with eucalypt overstory on sand plain is common. Halophytic vegetation occurs throughout the region on paleo-drainage systems, breakaways and on some stony and alluvial plains. Highly saline soils support Atriplex (saltbush), Maireana (bluebush) and Tecticornia (samphire) shrublands, while less saline soils support mulga with saltbush or bluebush understory
Threatened/Priority Flora	From a survey of the area in June 2021, <i>Eremophila arachnoides</i> subsp. <i>tenera</i> (priority 3, recently downgraded from priority 1) is located within the surveyed area. Closest individuals are approx. 500m north west of the TSF.
Threatened/Priority Fauna	Malleefowl are active on the Premises. A survey during June 2021 of the area to be covered by Cell 4 found no sightings of birds, 10 nesting mounds classed "long abandoned, 3 "recent failed", 4 "recent abandoned" and 4 "recent potentially active". The management of impact to this fauna is under the EPBC Act. Refer Section 2.4

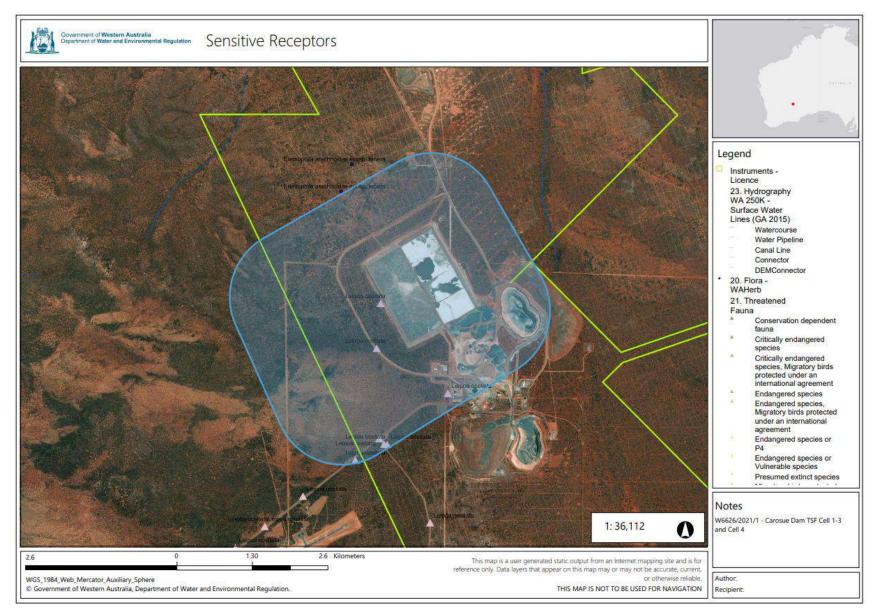


Figure 2: Distance to sensitive receptors using 1 km buffer

Works approval: W6626/2021/1

3.2 Risk ratings

Risk ratings have been assessed in accordance with the *Guideline: Risk Assessments* (DWER 2020) for each identified emission source and takes into account potential source-pathway and receptor linkages as identified in Section 3.1. Where linkages are in-complete they have not been considered further in the risk assessment.

Where the applicant has proposed mitigation measures/controls (as detailed in Section 3.1), these have been considered when determining the final risk rating. Where the delegated officer considers the applicant's proposed controls to be critical to maintaining an acceptable level of risk, these will be incorporated into the works approval as regulatory controls.

Additional regulatory controls may be imposed where the applicant's controls are not deemed sufficient. Where this is the case the need for additional controls will be documented and justified in Table 4.

Works approval W6626/2021/1 that accompanies this decision report authorises construction and time-limited operations. The conditions in the issued works approval, as outlined in Table 4 have been determined in accordance with *Guidance Statement: Setting Conditions* (DER 2015).

A licence is required following the time-limited operational phase authorised under the works approval to authorise emissions associated with the ongoing operation of the premises i.e. Category 5 activities. A risk assessment for the operational phase has been included in this decision report, however licence conditions will not be finalised until the department assesses the licence application.

Table 4: Risk assessment of potential emissions and discharges from the premises during construction and operation

Risk Event					Risk rating	Annelisant			
Source/Activities	Potential emissions	Potential pathways and impact	Receptors	Applicant controls	C = consequence L = likelihood	Applicant controls sufficient?	Conditions of works approval	Justification for additional regulatory controls	
Construction				·		·			
Construction of raises on Cell 3, construction of Cell 4 and amalgamation of Cell 1-2 with Cell 3 to form Cell 1-3	Dust	Air/windborne pathway causing impacts to health and amenity	Vegetation Fauna – mallee fowl nests	Refer to Section 3.1	C = Slight L = Unlikely Low Risk	Y	No specific conditions for dust management are required.		
Operation									
	Tailings Direct deposition from pipeline leaks	-	Refer to Section 3.1			Condition 1 – standard infrastructure and equipment condition. Includes position and dimensions of			
Transport of tailings and decant/recovered seepage through pipelines.	Decant/ seepage recovery water	or spills causing contamination of soil Contaminated soil causing contamination of stormwater. Direct deposition on surrounding vegetation.	Vegetation Fauna – mallee fowl nests Surface water		C = Moderate L = Possible Medium Risk	Y	stormwater management infrastructure and pipeline infrastructure. Conditions 5-6 – standard compliance report conditions Conditions 10 and 12 – standard conditions permitting operation of infrastructure for 180 days once constructed and reported.	Construction details proposed by the works approval holder are conditioned to minimise risk from leaks and spills during operation.	

Risk Event					Risk rating	Applicant		
Source/Activities	Potential emissions	Potential pathways and impact	Receptors	Applicant controls	C = consequence L = likelihood	controls sufficient?	Conditions of works approval	Justification for additional regulatory controls
Discharge of tailings	Tailings	Direct deposition from overtopping of TSF cells causing contamination of soil. Contaminated soil contaminating storm water runoff. Direct deposition on surrounding vegetation.	opping of causing tion ofVegetationC = Moderateted soil ting storm ff.Fauna - mallee fowl nestsL = PossibleMedium RiskMedium Risk	Y	Condition 2 – standard critical containment infrastructure condition. The 3 stages of TSF construction are detailed. Conditions 7-8 – standard critical containment infrastructure report conditions. Condition 11 – 13 standard conditions permitting operation of infrastructure for 180 days once constructed and reported.	Construction details proposed by the works approval holder are conditioned to minimise risk of overtopping. Conditions for operation of the TSF during limited time operations reflect the licence, L7465/1999/9, conditions already in place for the management of the TSF.		
to TSF.	Leachate	Seepage through ground into groundwater aquifers/creating perched groundwater aquifer. Surface expression of groundwater coming into contact with stormwater runoff. Mounding of groundwater into vegetation root zones	Groundwater aquifer Surface water Vegetation	Refer to Section 3.1	C = Moderate L = Unlikely Medium Risk	Y	Condition 2 – standard critical containment infrastructure condition. The 3 stages of TSF construction are detailed. Condition 3 – construction/installation condition for monitoring bores at the new TSF Cell 4. Conditions 7-8 – standard critical containment infrastructure report conditions. <u>Baseline</u> groundwater monitoring required	Refer to Section 3.3 Groundwater monitoring conditions for the new monitoring bores reflect the current licence, L7465/1999/9 conditions. This will enable the monitoring to be carried out and included with groundwater monitoring reporting for the whole TSF.

Works approval: W6626/2021/1

Risk Event			Risk rating	Applicant				
Source/Activities	Potential emissions	Potential pathways and impact	Receptors	Applicant controls	C = consequence	controls sufficient?	Conditions of works approval	Justification for additional regulatory controls
							for Cell 4 construction. Condition 11 – 13 standard conditions permitting operation of infrastructure for 180 days once constructed and reported. Condition 14 – monitoring of groundwater in new Cell 4 monitoring bores.	

Note 1: Consequence ratings, likelihood ratings and risk descriptions are detailed in the Guideline: Risk Assessments (DWER 2020).

Note 2: Proposed applicant controls are depicted by standard text. **Bold and underline text** depicts additional regulatory controls imposed by department.

3.3 Detailed risk assessment for seepage from Carosue Dam TSF

3.3.1 Background

The expansion of the TSF would cause vertical leakage of tailings water through the floor of the TSF and contribute to mounding of the water table in the underlying saprolite aquifer, which in turn would enhance migration of TSF seepage within the local aquifer system.

The pre-mining water table is estimated as 19–22 metres below ground level (mbgl) within the weathering profile underneath the TSF, based on early investigations from the Whirling Dervish area. Seepage from the TSF has caused groundwater mounding around 8 mbgl beneath the northeast corner of the TSF whilst mining has produced a groundwater depression of 199 mbgl in the nearby Whirling Dervish Pit.

Seepage can potentially waterlog the root zone of vegetation causing health impacts and surface expression of seepage can potentially contaminate stormwater runoff. To mitigate these impacts the works approval holder engaged the consultant Pennington Scott to design appropriate TSF seepage recovery as necessary to ensure that there is no risk of waterlogging (water table less than 6 mbgl) or offsite TSF seepage migration off the works approval holder's tenements.

The licence for the premise, L7465/1999/9, establishes the following groundwater quality limits in condition 23 to control potential impacts of seepage on the environment:

- SWL = >4.0 mbgl
- Weak acid dissociable cyanide (WADCN) <0.5 mg/L

As per condition 23 if any limit is not met then the result must be investigated. Under condition 24 if the WADCN limit is exceeded then a Groundwater Recovery Plan must be designed and implemented. Condition 8 of the licence also requires that, upon becoming aware that depth to groundwater levels in monitoring bores around the TSF are less than 6.0 mbgl, then the works approval holder, within six months, must design and implement a Groundwater Recovery Plan.

The Groundwater Recovery Plan must meet the requirements of Condition 9 which include the developing of strategies to achieve and maintain the groundwater below the level limits. The works approval holder uses 6mbgl as a trigger to initiate actions before the SWL >4 mbgl limit is reached.

A recovery plan has not had to be implemented to date as the limit has not been exceeded. Modelling provided with the application for this works approval indicates that the SWL trigger value may be exceeded after 10 years and in worse case scenarios with the operation of Cell 4 and Cell 1 -3 without any TSF recovery bores.

3.3.2 Water balance

Figure 3 provides a water balance for the current TSF and associated processing infrastructure using the current figures. This water balance, as provided by the works approval holder with the application supporting document, does not include the inflow of rainfall. Rainfall inflow is however a small percentage of the inflow to the TSF and the tailings thickener removes approximately 54% of the water from the tailings prior to discharge and returns it to the process stream or the paste fill plant. Approximately 25% (49,000kL/month) of all water sent to the Tailings Storage facility is returned to the Process Plant for reuse through underdrainage and decant return pumps. An estimated 5% of the water in tailings is released as seepage with the remainder lost to evaporation and moisture retention.

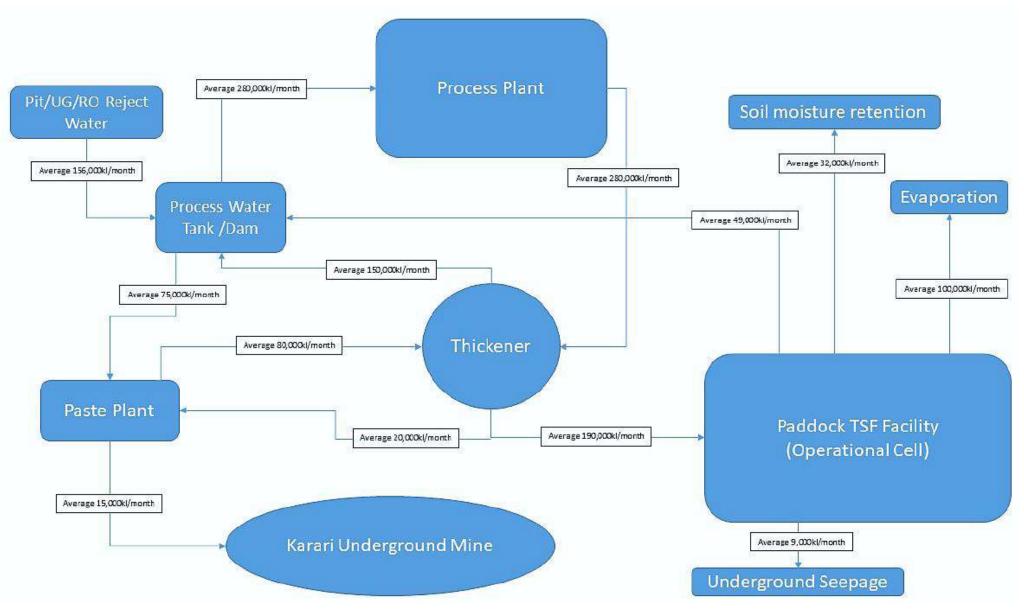


Figure 3: Water balance for the current TSF and associated processing infrastructure (unit = kL/month)

Works approval: W6626/2021/1

Future water balance estimates were provided in the TSF design report by Coffey (2021) and shown in Table 5 below. The water balance provided by Coffey does provide the same estimates as provided by the works approval holder in Figure 4. The water balance provided by Coffey however reflects estimates based on expected future conditions at the final stages of the TSF cells.

The results of the water balance analysis indicated:

• For Cell 3 Stage 4, an estimated annual water return of approximately 0.311 Mm3, which equates to 21% of annual slurry water inflow (i.e. 1.51 Mm3). The average water shortfall (or makeup water) is estimated at 1.20 Mm3/year.

• For Super Cell 1-3 Stage 4 (final stage), an estimated annual water return of approximately 0.388 Mm3, which equates to 18.0% of annual slurry water inflow (i.e. 2.21 Mm3). The average water shortfall (or makeup water) is estimated at 1.82 Mm3/year.

• For Cell 4 Stage 4 (final stage), an estimated annual water return of approximately 0.452 Mm3, which equates to 19.0% of annual slurry water inflow (i.e. 2.21 Mm3). The average water shortfall (or makeup water) is estimated at 1.78 Mm3/year.

Table 5: TSF annual water balance summary

Inflows (m³/ye	ar)	Outflows (m³/year)				
Cell 3 Stage 4 Operation						
Rainfall	104,906	Evaporation	434,128			
Slurry water	1,507,692	Evapotranspiration	14,851			
		Seepage	15,688			
		Retention	840,000			
Total inflow	1,612,599	Total outflow	1,304,667			
		Return water	311,031m³/year			
Average water shortfall (or make up v	Average water shortfall (or make up water) = Slurry (inflow) water – Return water					

Super Cell 1-3 Stage 4 Operation

Rainfall	185,455	Evaporation	738,566		
Slurry water	2,207,692	Evapotranspiration	27,949		
		Seepage	42,274		
		Retention	1,230,000		
Total inflow	2,393,147	Total outflow	2,038,789		
		Return water	388,081m³/year		
Average water shortfall (or make up water) = Slurry (inflow) water – Return water 1,819,612m³/year					

Cell 4 Stage 4 Operation						
Rainfall	170,916	Evaporation	709,537			
Slurry water	2,207,692	Evapotranspiration	24,064			
		Seepage	10,906			
		Retention	1,230,000			
Total inflow	2,378,608	Total outflow	1,974,507			
		Return water	452,304m³/year			
Average water shortfall (or make up	1,782,388m³/year					

Works approval: W6626/2021/1

3.3.3 Current TSF seepage management

Seepage from Carosue Dam TSF is historically managed by a tailings thickener reducing the water content prior to discharge to the TSF and differing underdrainage systems under the cells. Cells 1 and 2 were constructed with partial underdrainage and Cell 3 with underdrainage under the decant pond area. Cells 1 and 2 were merged as one cell in 2019 at Stage 7 of both cells design. The Carosue Dam Thickener also directly returns approximately 150,000kl per month of water to the processing circuit which would otherwise report directly to the TSF.

The TSF seepage rate has been steadily declining since the start of mining as the groundwater mound has developed. During the initial wetting phase, the TSF would have been losing up to 8L/s through its base, which has declined to its current rate of around 3.5L/s. Although there appears to be significant groundwater mounding around the TSF, the actual volumes of TSF seepage may be very low due to the low permeability of the clayey upper saprolite horizon. The TSF is also in close vicinity to Whirling Dervish Pit and recirculation of TSF seepage is believed to account for about 10% of the dewatering from Whirling Dervish.

The pre-mining water table was initially observed around 19–22 mbgl within the weathering profile underneath the TSF, based on early investigations from the Whirling Dervish area. Figure 4 illustrates the impact of the Whirling Dervish Pit on the groundwater flow around the existing TSF. The pit creates a sink that the seepage flows towards. The seepage on the northern edge of the TSF, where mounding is up to 7.85mbgl, is also expected to report to the pit in the long term. The expected post closure state of the pit is that it will partially fill with water and remain a groundwater sink.

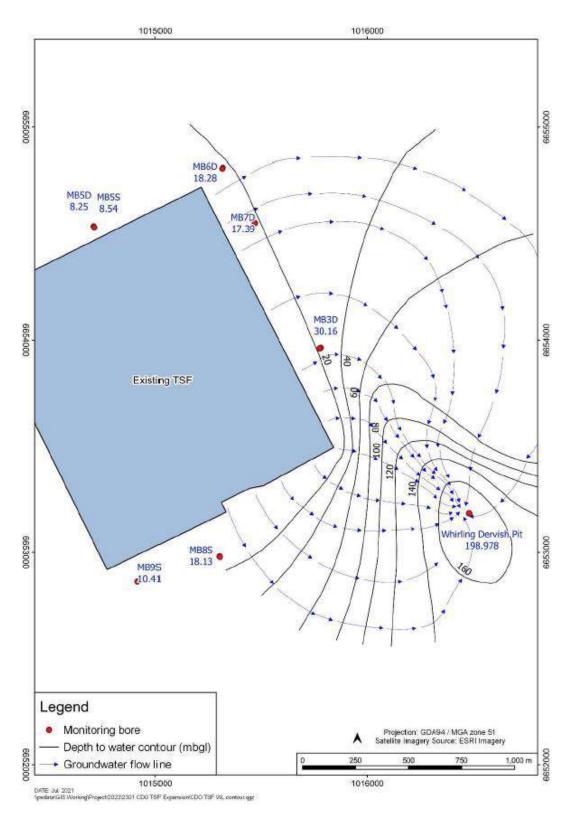


Figure 4: Depth to water contour around TSF and Whirling Dervish – February to August

3.3.4 Estimated seepage from proposed construction of Cell 4 and Cell 1-3

A surface and groundwater hydrological study for the TSF expansion looked at the future seepage transport from the TSF. The expansion of the TSF will cause vertical leakage of tailings water through the floor of the TSF and contribute to mounding of the water table in the underlying saprolite aquifer, which in turn would enhance migration of TSF seepage within the local aquifer system. The seepage rate from the proposed Cell 4 and Cell 1-3 arrangement of the TSF has been modelled using scenarios of seepage without recovery bores and seepage with recovery bores. Other controls currently mitigating seepage impacts from the TSF will remain in place.

The results of the seepage analyses indicated that total seepage from the TSF final stages would range between approximately 30 and 115 m3/d under normal operating conditions. The introduction of underdrainage system at the basin floor is anticipated to reduce the seepage losses through the basin floor area.

The estimated shallowest SWLs around the TSF after 10 years for both scenarios are shown in Figure 5 and Figure 6.

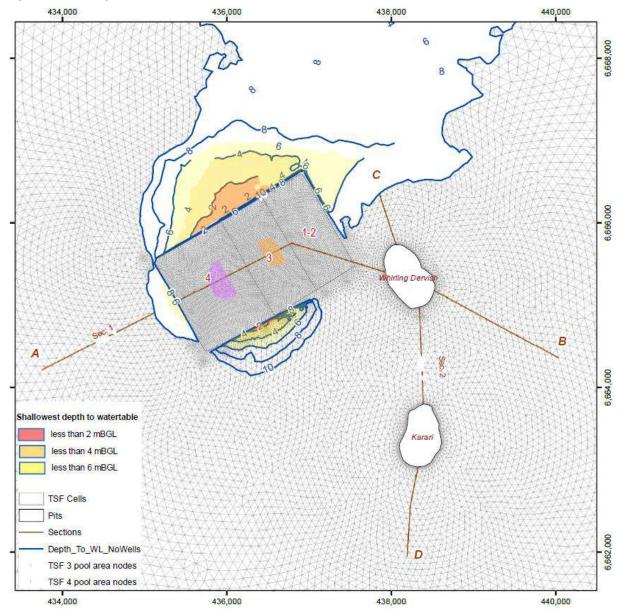


Figure 5: Estimated depth to groundwater after 10 years without recovery bores

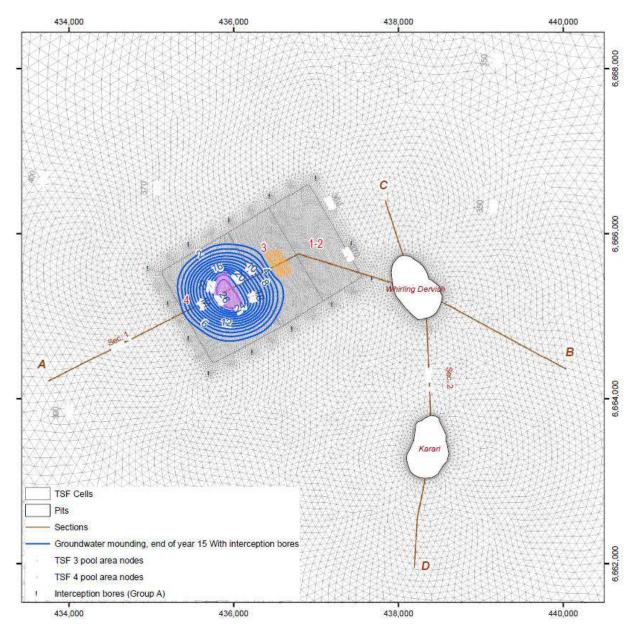


Figure 6: Estimated depth to groundwater after 10 years with recovery bores

3.3.5 Risk rating of seepage

The risk of the seepage causing impact on vegetation and surface water has been assessed previously as requiring licence conditions setting of a SWL limit of >4mbgl and a WADCN limit of <0.5mg/L. To avoid being non-compliant with the SWL limit the works approval holder has set a trigger level in their seepage management plan of 6mbgl. Modelling of the seepage from the TSF, assuming no recovery bores are installed, shows that both the trigger level and the limit will be exceeded within 10 years. Modelling of the same seepage over the same timeframe with recovery bores shows that the controls will effectively manage the seepage.

Consequence of seepage impacting the environment = Moderate

Likelihood of seepage impacting the environment with controls in place = unlikely

Consultation

Table 6 provides a summary of the consultation undertaken by the department.

Table 6: Consultation

Consultation method	Comments received	Department response
Application advertised on the department's website on 7/01/2022	None received	N/A
Application advertised in <i>West Australian</i> newspaper on 10/01/2022	None received	N/A
Local Government Authority (Shire of Menzies) advised of proposal on 7/01/2022	None received	N/A
Local Government Authority (City of Kalgoorlie-Boulder) advised of proposal on 7/01/2022	None received	N/A
Department of Mines, Industry Regulation and Safety (DMIRS) advised of proposal 7/01/2022	DMIRS replied on 19/01/2022 advising that: This works approval application is consistent with a mining proposal currently under assessment (on hold pending additional information from proponent) by DMIRS (Reg. ID: 101504). During the assessment of this mining proposal, a DMIRS Inspector of Mines – Geotechnical, reviewed the application and advised that geotechnical aspects had been sufficiently considered by the proponent. The assessing officer has raised questions regarding some environmental aspects of the mining proposal, however none that are specifically related to the TSF.	No response required.
Applicant was provided with draft documents on 3 June 2022	Updated premises map and Mallee fowl assessment provided. Details of Cell 1-3 decant were confirmed.	The decision report and works approval conditions were updated as necessary with the information provided.

4. Conclusion

Based on the assessment in this decision report, the delegated officer has determined that a works approval will be granted, subject to conditions commensurate with the determined controls and necessary for administration and reporting requirements.

References

- 1. Department of Environment Regulation (DER) 2015, *Guidance Statement: Setting Conditions*, Perth, Western Australia.
- 2. Department of Water and Environmental Regulation (DWER) 2020, *Guideline: Environmental Siting*, Perth, Western Australia.
- 3. DWER 2020, Guideline: Risk Assessments, Perth, Western Australia.
- 4. Tetra Tech Coffey (Coffey 2021), *Carosue Dam Gold Mine TSF Cell 1-3 and Cell 4 Design Report*, Perth, Western Australia.
- 5. Pennington Scott (2021), Surface and Groundwater Hydrological Studies for Life of Mine TSF Expansion Project: Carosue Dam Operations, Perth, Western Australia.

Appendix 1: Design and construction of Cell 1-3 and Cell 4

1. Cell 1-3 Design

The TSF cells currently have the arrangement of a two cell facility: Cell 1-2 and Cell 3, Figure 7. Cell 1-2 was created when Cell 1 and Cell 2 both reached Stage 7 of their design heights and the merged cell has just been raised to Stage 8 (RL381).

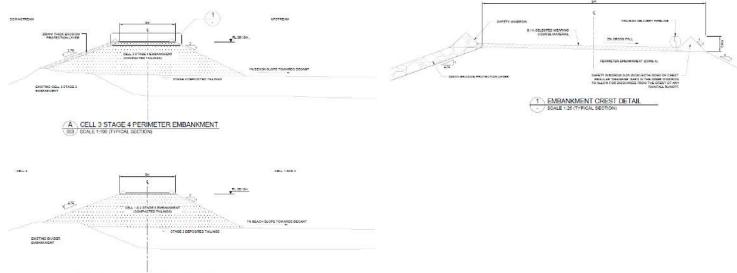
With this works approval Cell 3 will be raised to an embankment crest level of RL 381 m, Stage 4 of the cell design. Once Stage 4 of Cell 3 has been filled with tailings and sufficiently dried the two current cells will be combined with one lift into Cell 1-3, Stage 1.



Figure 7: Current TSF cells. Cell 1-2 and Cell 3

1.1 Stage 4 of Cell 3

Stage 4 of Cell 3 will be an upstream lift of the outer embankments using dried tailings from Stage 3 of Cell 3 and an outer, erosion protection layer of waste rock. The divider embankment between Cells 1-2 and 3 will be the embankment of the Cell 1-2 Stage 8 raise.



B CELL 182 STAGE 8 DIVIDER EMBANKMENT

Figure 8: Embankment design for Cell 3, Stage 4

The arrangement of pipelines, decant tower and spigots will be as per Cell 3, Stage 3. Figure 9

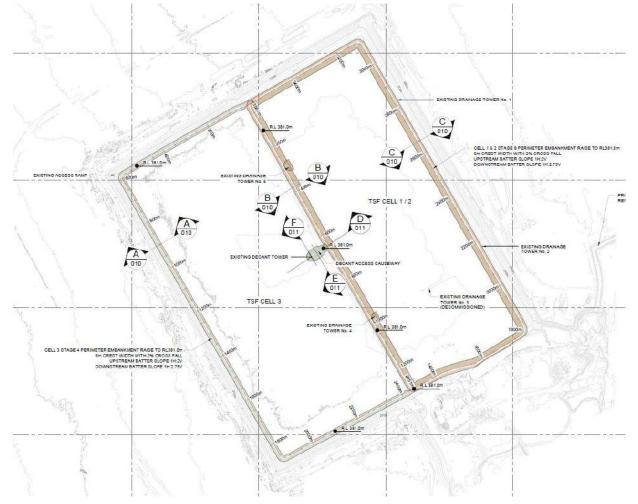


Figure 9: Cell 3, Stage 4

1.2 Cell 1-3

Works approval: W6626/2021/1

The combining of the TSF cells Cell 1-2 and Cell 3 to form a super cell Cell1-3 will require the removal of existing drainage towers 4 and 5 as the dividing wall will be buried under tailings. The current Cell 3 decant structure will be retained and raised as the new Cell 1-3 decant structure. A new causeway to the decant will extend from the west wall of the cell, that is the dividing wall between the new Cell 4 and the super cell.

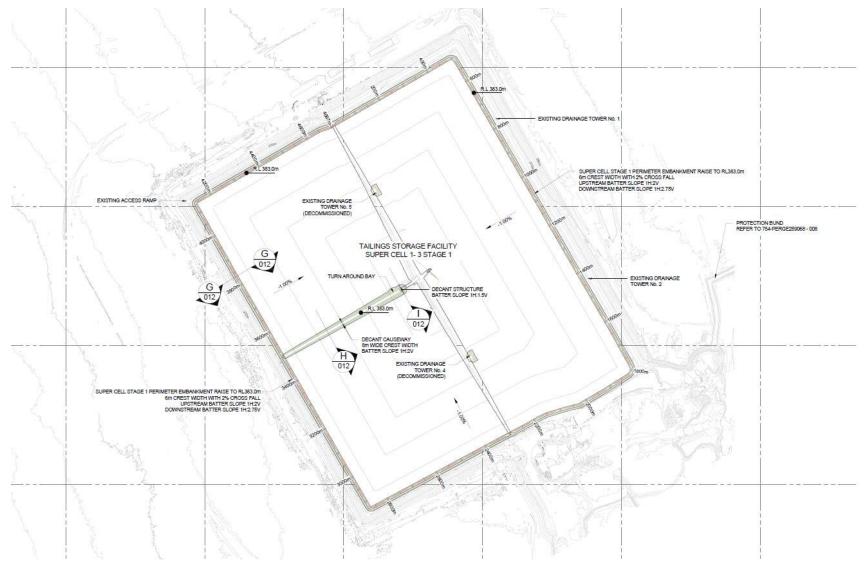


Figure 10: Cell 1-3 design

Works approval: W6626/2021/1

2. Cell 4 Design

Cell 4 is a paddock-type storage facility with a storage surface area of approximately 120.7 ha, abutting the southwest side of the existing Cell 3. The cell will include:

- soil surface compacted after topsoil stripping. Ground permeability beneath proposed TSF 4 tested to less than 1x10⁻⁷ m/s;
- walls constructed from compacted clay mine waste to a height of RL 375.5m Figure 11 and Figure 12;
- cut off trench at base of wall 2m deep and 4m wide at base and filled with compacted clay mine waste Figure 12;
- a decant constructed from a slotted concrete pipe and clean rock fill filter, RL 372.5m.
 Decant causeway constructed with mine waste to RL372.5m Figure 13;
- underdrainage across the entire base of the cell Figure 14;
- a return water pond to collect outflow from underdrainage, lined with geotextile and HDPE Figure 15;
- 6 monitoring bores and 12 vibrating wire piezometers Figure 16;.

Construction will include stripping of topsoil and compacting the base of the TSF to a permeability greater than 1×10^{-7} m/s. A cut off trench and underdrainage will be installed, and the wall is constructed using compacted clay mine waste.

The underdrainage lines will comprise slotted pipe (Megaflo 150 and 450 - slotted composite panel drain) covered in filter sand / fine aggregate wrapped in geotextile and stabilised with coarse aggregate or select rockfill. The underdrainage pipe will be placed above the stripping level. Underdrainage water collected via the underdrainage piping system will drain by gravity to an internal underdrainage sump. The minimum designated fall/gradient of the underdrainage pipe is 0.2%. The underdrainage sump will be located immediately adjacent to the upstream embankment toe, at the lowest point within the Cell 4 basin area (i.e. at the south-east corner).

Underdrainage water in the underdrainage sump will be recovered via an inclined riser pipe (DN 315 mm HDPE casing) housing a submersible pump (designed by others) to handle an estimated maximum flow of 2 L/s (or 165 m₃/day) under normal operating conditions.

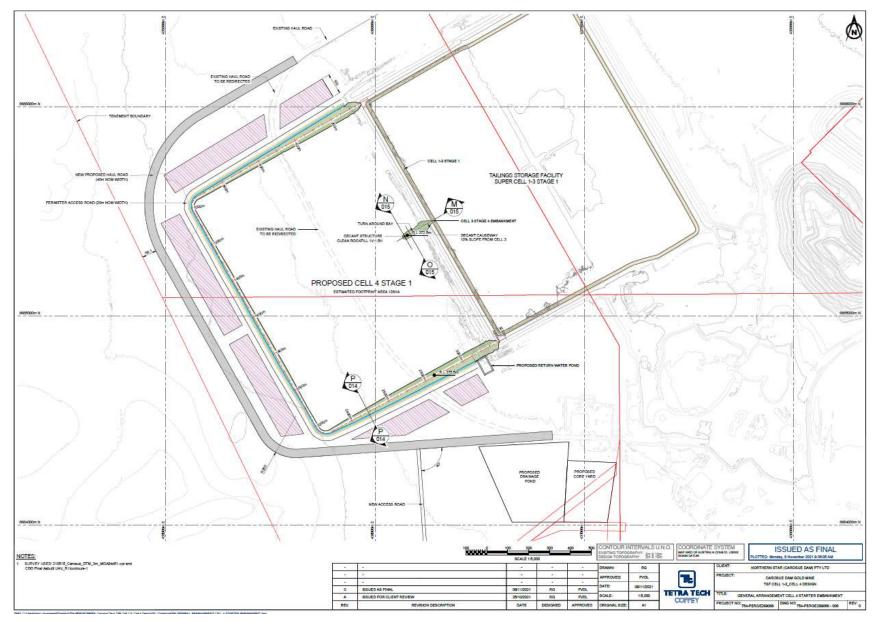


Figure 11: Cell 4 design

Works approval: W6626/2021/1

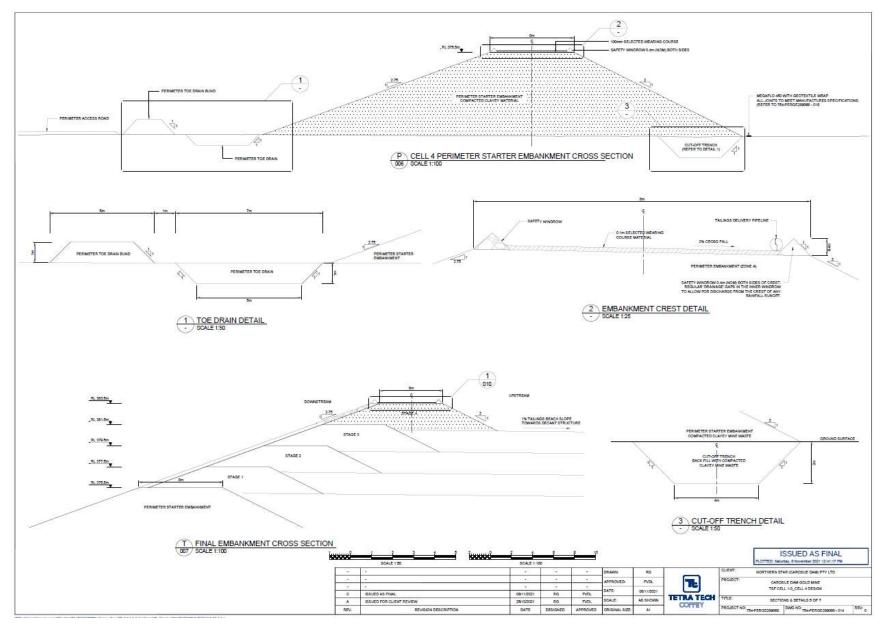


Figure 12: Perimeter wall design with toe drain and cut off trench details

Works approval: W6626/2021/1

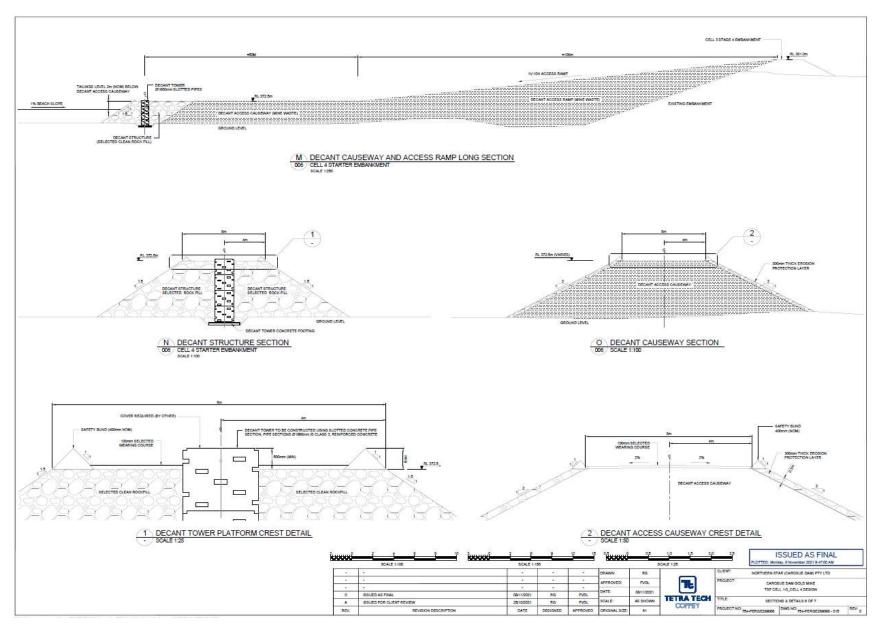


Figure 13: Decant structure and decant causeway

Works approval: W6626/2021/1

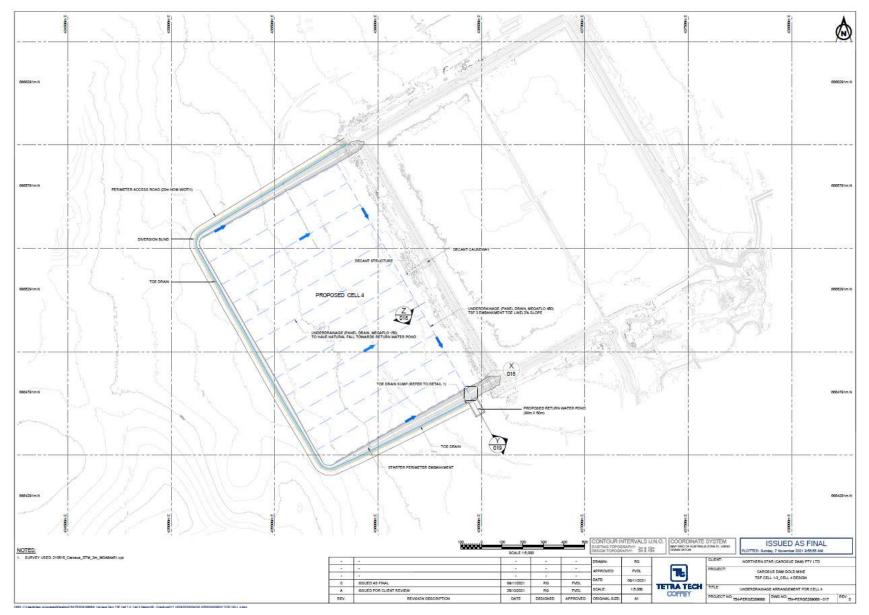


Figure 14: Underdrainage

Works approval: W6626/2021/1

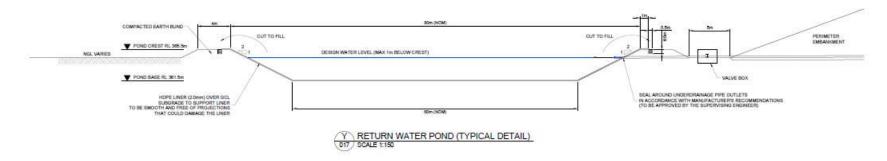


Figure 15: Return water pond to capture underdrainage

Works approval: W6626/2021/1

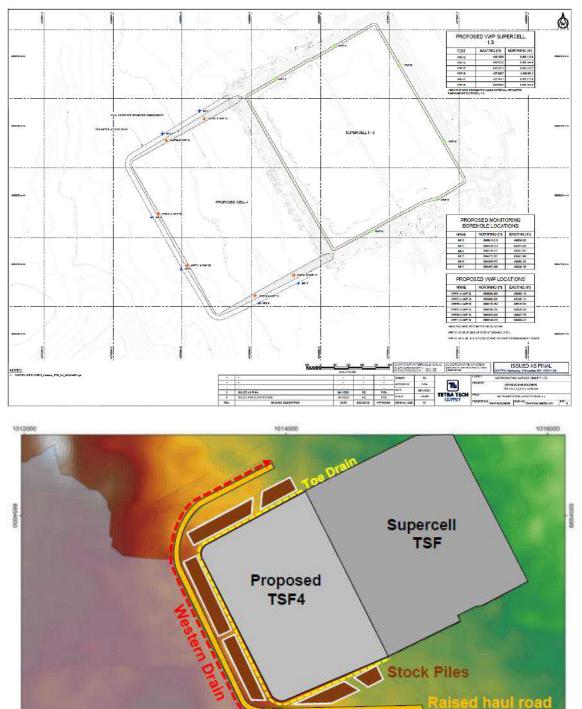


Figure 16: Monitoring bores and piezometers

Works approval: W6626/2021/1

3. Final cell arrangement of TSF

The final TSF will be a two cell paddock style TSF with stormwater diverted around the southern walls to the west and the south east.



IN TAXABLE INCOME ADDR. NAME

Southern Drain

101400

100 ML

Drainage pond

0

250

500

750

1.00

Appendix 2: Application validation summary

SECTION 1: APPLICATION SUMMARY (as updated from validation checklist)						
Application type						
Works approval	\boxtimes					
		Relevant works approval number:			None	
		Has the works approva with?	I been complied	Yes	Yes 🗆 No 🗆	
Licence		Has time limited operations under the works approval demonstrated acceptable operations?Yes □ No □		□ N/A □		
		Environmental Complia Critical Containment In Report submitted?				
		Date report received:				
Renewal		Current licence number:				
Amendment to works approval		Current works approval number:				
Amendment to licence		Current licence number:				
Amendment to licence		Relevant works approval number:			N/A	
Registration		Current works approval number:	None			
Date application received		19/11/2021				
Applicant and premises details						
Applicant name/s (full legal name/s)		Northern Star Resource 116649122	es (Carosue Dam) F	Pty L	td. ACN	
Premises name		Carosue Dam Minesite	•			
Premises location		M28/269, M31/220, M31/295				
Local Government Authority		Shire of Menzies				
Application documents						
HPCM file reference number:		DER2021/000666				
Key application documents (addition application form):	DWERDT529321: Cl Supporting Info_FIN/		Cell	4 LOM	TSF	

Scone of application/accoment		s updated from validation of				
Scope of application/assessment						
		Mine tailings management	-3 Raises & Cell 4 developed for Life o			
		 Stage 4 of existing Cell 3 will be raised to an embankment crest level of RL 381 m; 				
Summary of proposed activities or		the west of existing enclose an interna	developed as a paddock-type facility to Cell 3. A perimeter embankment to I impoundment surface area o at starter embankment crest elevation constructed;			
changes to existing operations.		3. Merging of Cells 1-2 ar level of RL 383 m;	nd Cell 3 to form a Supercell 1-3 at cres			
		constructed at Cell 4 v	upstream raised embankment will be vith a final embankment crest elevatior Stage 1 to Stage 4); and			
		 A further 3 stages of upstream raised embankment will l construction at Supercell 1-3 with final embankment cre elevation of RL 389 m (Supercell 1-3 Stage 2 to Stage 4). 				
Category number/s (activities that caus	se the	premises to become prescri	bed premises)			
5 <i>,</i>			. ,			
Table 1: Prescribed premises categorie	es					
		essed production or ign capacity	Proposed changes to the			
		.g c.p	production or design capacity (amendments only)			
Category 5: Processing and beneficiation of metallic or non- metallic ore		0,000 tonnes per annual				
beneficiation of metallic or non- metallic ore	4,00 perio	0,000 tonnes per annual	(amendments only)			
beneficiation of metallic or non- metallic ore	4,00 perio	0,000 tonnes per annual	(amendments only)			
beneficiation of metallic or non- metallic ore Legislative context and other approv Has the applicant referred, or do they	4,00 perio vals	0,000 tonnes per annual	(amendments only)			
beneficiation of metallic or non- metallic ore Legislative context and other approv Has the applicant referred, or do they intend to refer, their proposal to the E	4,00 perio vals	0,000 tonnes per annual	(amendments only)			
beneficiation of metallic or non- metallic ore Legislative context and other approv Has the applicant referred, or do they	4,00 perio vals	0,000 tonnes per annual od	(amendments only) N/A Referral decision No:			
beneficiation of metallic or non- metallic ore Legislative context and other approv Has the applicant referred, or do they intend to refer, their proposal to the E under Part IV of the EP Act as a significant proposal?	4,00 perio vals	0,000 tonnes per annual od	(amendments only) N/A Referral decision No: Managed under Part V □			
beneficiation of metallic or non- metallic ore Legislative context and other approv Has the applicant referred, or do they intend to refer, their proposal to the E under Part IV of the EP Act as a	4,00 perio vals PA	0,000 tonnes per annual od	(amendments only) N/A Referral decision No: Managed under Part V □ Assessed under Part IV □			
beneficiation of metallic or non- metallic ore Legislative context and other approved Has the applicant referred, or do they intend to refer, their proposal to the E under Part IV of the EP Act as a significant proposal? Does the applicant hold any existing F IV Ministerial Statements relevant to t	4,00 perio vals PA	0,000 tonnes per annual od Yes □ No ⊠	(amendments only) N/A N/A Referral decision No: Managed under Part V □ Assessed under Part IV □ Ministerial statement No:			

SECTION 1: APPLICATION SUMMARY (as	s updated from validation	checklist)
Has the applicant demonstrated occupancy (proof of occupier status)?	Yes 🛛 No 🗆	Mining lease / tenement ⊠ Expiry: M28/269 (Expires 01/05/2029), M31/220 (Expires 14/7/2041) M31/295 (Expires 01/05/2029)
Has the applicant obtained all relevant planning approvals?	Yes 🗆 No 🗆 N/A 🖂	If N/A explain why? Mining tenure
Has the applicant applied for, or have an existing EP Act clearing permit in relation to this proposal?	Yes ⊠ No □	CPS No: 8000/2 is under assessment.
Has the applicant applied for, or have an existing CAWS Act clearing licence in relation to this proposal?	Yes 🗆 No 🖂	Application reference No: N/A Licence/permit No: N/A No clearing is proposed.
Has the applicant applied for, or have an existing RIWI Act licence or permit in relation to this proposal?	Yes 🗵 No 🗆	Licence/permit No: GWL157428(5)
Does the proposal involve a discharge of waste into a designated area (as defined in section 57 of the EP Act)?	Yes ⊠ No □	 Name: Goldfields Type: Proclaimed Groundwater Area Has Regulatory Services (Water) been consulted? Yes □ No ⊠ N/A □ Regional office: Goldfields
Is the Premises situated in a Public Drinking Water Source Area (PDWSA)?	Yes □ No ⊠	Name: N/A Priority: N/A Are the proposed activities/ landuse compatible with the PDWSA (refer to <u>WQPN 25</u>)? Yes No N/A
Is the Premises subject to any other Acts or subsidiary regulations (e.g. <i>Dangerous</i> <i>Goods Safety Act 2004, Environmental</i> <i>Protection (Controlled Waste) Regulations</i> <i>2004, State Agreement Act xxxx</i>)	Yes ⊠ No □	Mining Act 1978 Rights in Water and Irrigation Act 1914

SECTION 1: APPLICATION SUMMARY (as updated from validation checklist)							
Is the Premises within an Environmental Protection Policy (EPP) Area?	Yes □ No ⊠						
Is the Premises subject to any EPP requirements?	Yes □ No ⊠						
Is the Premises a known or suspected contaminated site under the <i>Contaminated Sites Act 2003</i> ?	Vac M Na 🗆	Mining tenement M31/220 Classification: N/A – awaiting classification Date of classification: N/A					
	Yes ⊠ No □						