Fremantle METALLURGY
IT'S ALL ABOUT THE PROCESS

13B Weatherburn Way

Kardinya 6163

Western Australia

Talison Lithium

Greenbushes

(Particle Size Distribution and Rheology Testwork)

November 2025

CONFIDENTIALITY AND DISCLAIMER

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GRAPHS

1 Introduction

Talison Lithium Greenbushes is one of the world's premier lithium operations, located in Western Australia's South-West region 250km from Perth. As the longest continuously operated mining area for Western Australia, Greenbushes has a rich history dating back to the late 1888s. Today, it is recognized as a leading producer of high-grade lithium concentrate, which is a critical raw material for lithium-ion batteries used in electric vehicles, energy storage systems, and a variety of consumer electronics.

Managed by Talison Lithium, a joint venture between Tianqi Lithium, IGO and Albemarle Corporation, the Greenbushes mine is renowned for its extensive resources and significant contribution to meeting the growing global demand for lithium.

Talison have engaged Fremantle Metallurgy to complete particle size distribution and rheological testwork on their CGP1, CGP2, TRP and TGP tailings slurries.

2 Sample Receipt and Preparation

The samples received by Fremantle Metallurgy as part of FM2546 were used for PSD and rheology study. The samples were used 'as received'. The percentage of solids in the slurries is at 34% - CGP1, 33.8% - CGP2, 42.2% - TRP and 3.8% - TGP. All %solids contents were determined by oven drying sub-samples at 105°C overnight.

Figure 1: Samples Received

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3 Particle Size Distribution (Sieve analysis)

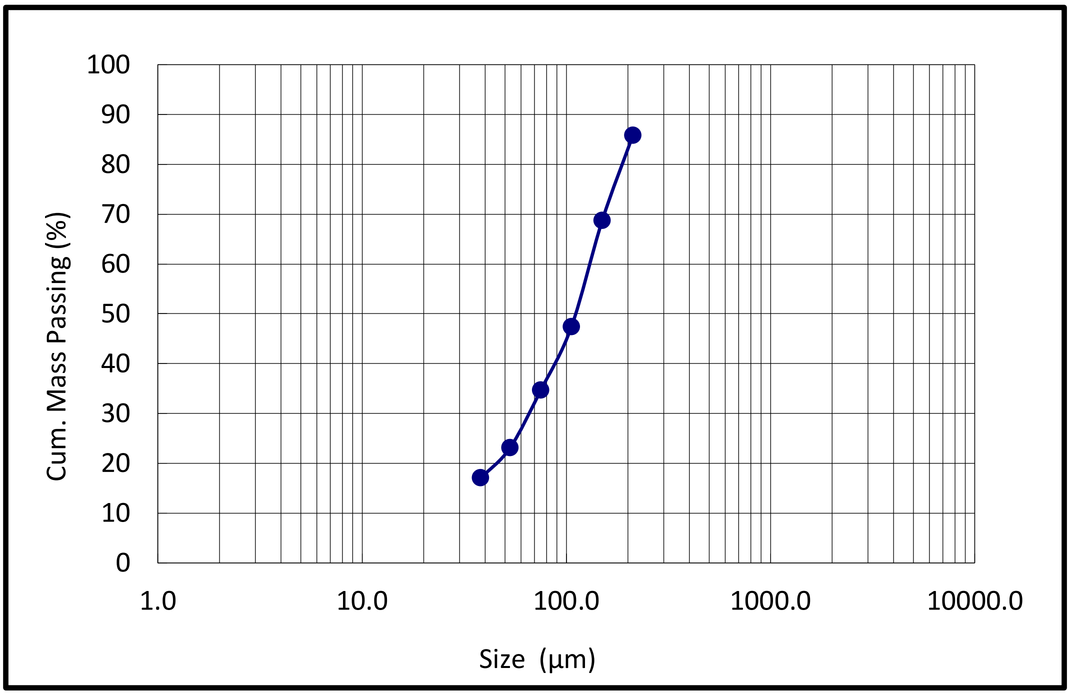
The samples were screened between 212 µm and 25 µm using standard Endecotts ISO test sieves. The results are provided below and display the %mass of particles passing each sieve size, as well as interpolated values for P80 and P50.

3.1 CGP1

Table 1: Sieve Analysis CGP1

Size (µm)	(%) Passing
212	85.8
150	68.7
106	47.4
75	34.6
53	23.1
38	17.0
-38	0.0
P80 (µm)	190.9
P50 (µm)	111.4

Graph 1: Size Distribution Curve CGP1

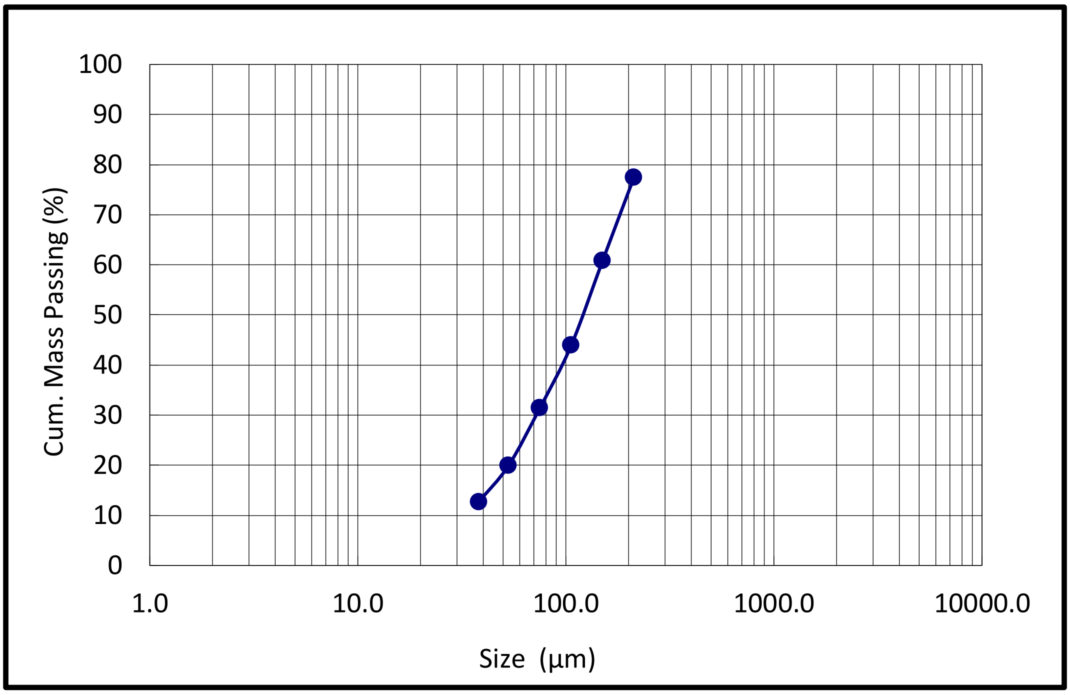


3.2 CGP2

Table 2: Sieve Analysis CGP2

Size (µm)	(%) Passing
212	77.3
150	60.8
106	43.9
75	31.4
53	19.9
38	12.6
-38	0.0
P80 (µm)	221.9
P50 (µm)	121.9

Graph 2: Size Distribution Curve CGP1

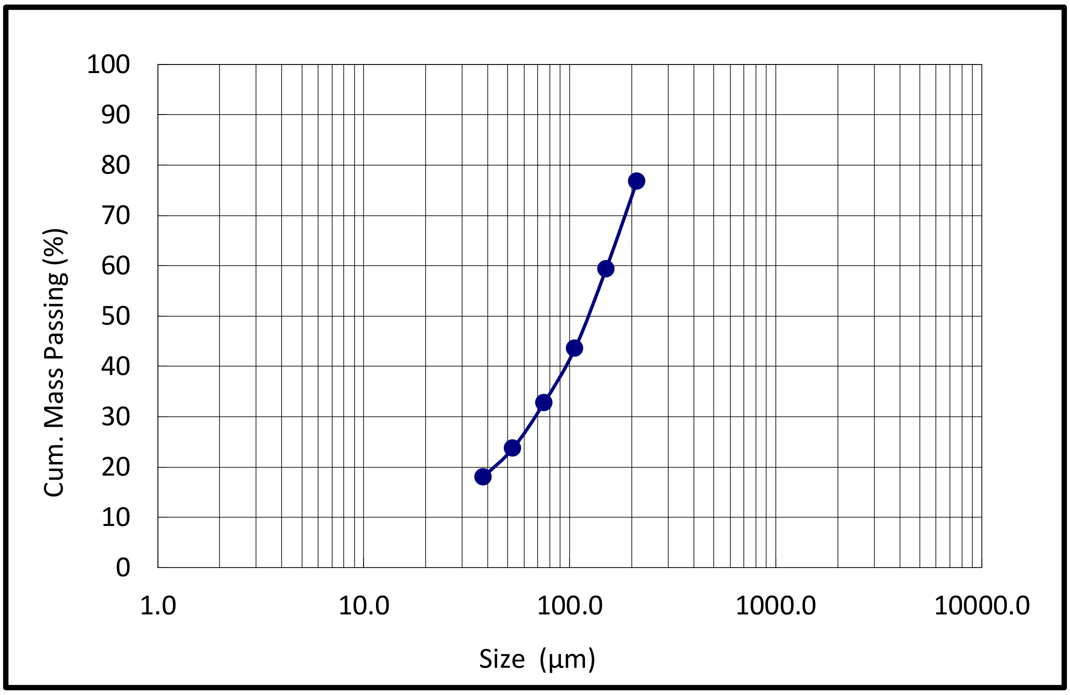


3.3 TGP

Table 3: Sieve Analysis TGP

Size (µm)	(%) Passing
212	76.8
150	59.3
106	43.5
75	32.7
53	23.7
38	18.0
-38	0.0
P80 (µm)	223.4
P50 (µm)	124.0

Graph 3: Size Distribution Curve TGP



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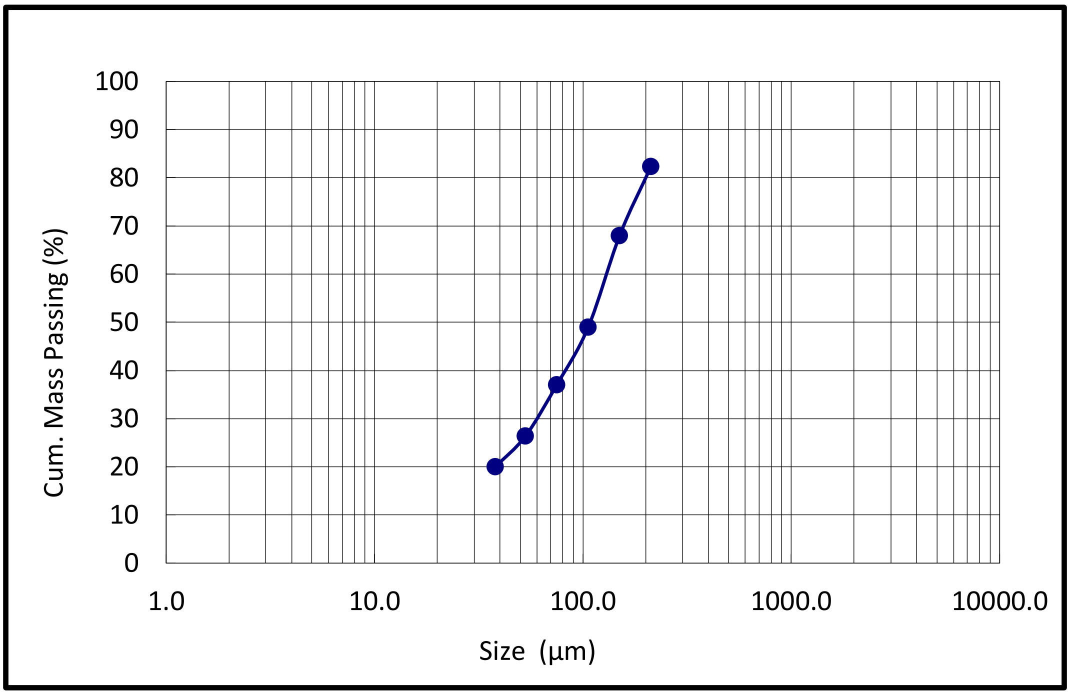
3.4 TRP

Table 4: Sieve Analysis TRP

Size (µm)	(%) Passing
212	82.3
150	68.0
106	49.0
75	37.1
53	26.4
38	20.0
-38	0.0
P80 (µm)	202.0
P50 (µm)	108.4

Graph 4: Size Distribution Curve TRP



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4 Rheology

Rheology testing was carried out using a Haake ViscoTester VTiQ, equipped with a profiled bob and cup configuration suitable for mineral slurries. Torque was measured across a programmed shear rate ramp from ~0.3 to 270s^{-1}, generating rheograms of shear stress versus shear rate. Apparent viscosity was calculated directly, and the data were fitted using the Bingham Plastic model to derive yield stress and plastic viscosity parameters where possible. At the lowest tested solids for each stream (≈34–42% for CGP1/CGP2/TRP and 3.8% for TGP), stresses and apparent viscosities remain low and yield stresses from Bingham fits were non-determinable.

Figure 2: The Haake ViscoTester iQ

Raw torque, shear stress and apparent viscosity data is provided in the Section 7 Appendix.

The rheology figures and tables present the processed output from the Haake ViscoTester VTiQ cup and bob tests on the four tailings streams. During each test, the instrument applied a programmed shear rate ramp of ~0.3-270 s^{-1} while measuring raw torque on a custom profiled bob. This bob features grooves cut along its length to help maintain suspension of the coarser particles, minimising settling effects.

The raw torque readings were converted to shear stress using the known geometry factors of the profiled bob and matching cup, and to apparent viscosity by dividing shear stress by the applied shear rate at each step in the ramp.

These processed values are presented in the torque, shear stress and apparent viscosity tables, and plotted as rheograms (shear stress vs shear rate) and viscosity curves (apparent viscosity vs shear rate) for each solids concentration.

For the Bingham analysis, the stress rate data for each slurry condition were fitted to the Bingham Plastic model ($\tau = \tau_y + K_B\dot{\gamma}$) using a linear fit over the near-linear portion of the rheogram excluding very low shear data where start up artefacts are most pronounced.

The intercept of this best fit line is reported as the Bingham yield stress (τ_y), and the slope as the Bingham modelled plastic viscosity (K_B), with the resulting parameters summarised in the Bingham model output tables alongside the raw rheogram and viscosity curve data.

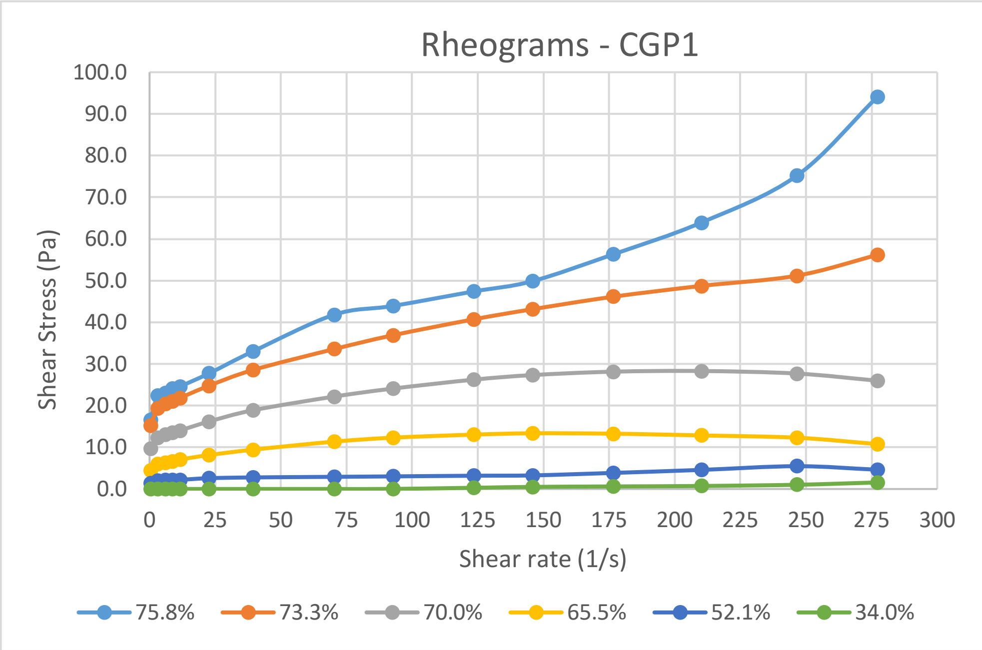
Yield stress and plastic viscosity for each solids concentration were plotted against %solids, and regression trendlines with their corresponding equations were added to allow interpolation of rheological behaviour at solids concentrations that were not directly tested.

Note: Although the “as received” solids contents for CGP1, CGP2, TRP and TGP were generally on the lower side, the slurries were quite fluid at these concentrations and produced only low stresses and viscosities.

To better define how the samples behaved under more demanding conditions, the rheology testing was therefore carried out at much higher solids levels than was received which is why there are sometimes large increments between the tested solids concentrations in the Bingham data.

4.1 CGP1

Graph 5: Rheograms – CGP1



Graph 6: Viscosity Curves – CGP1

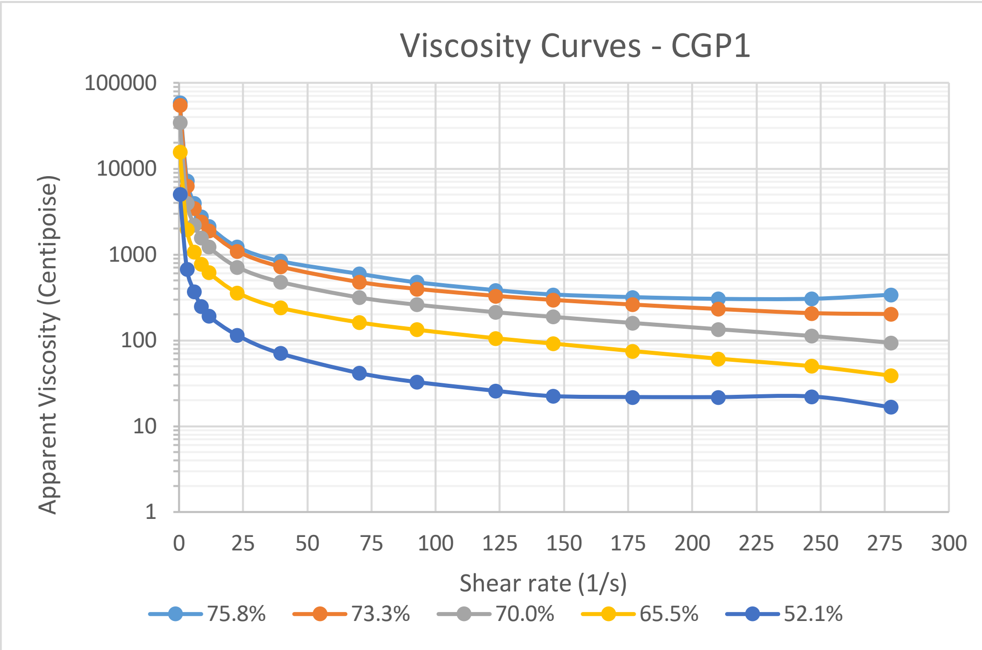
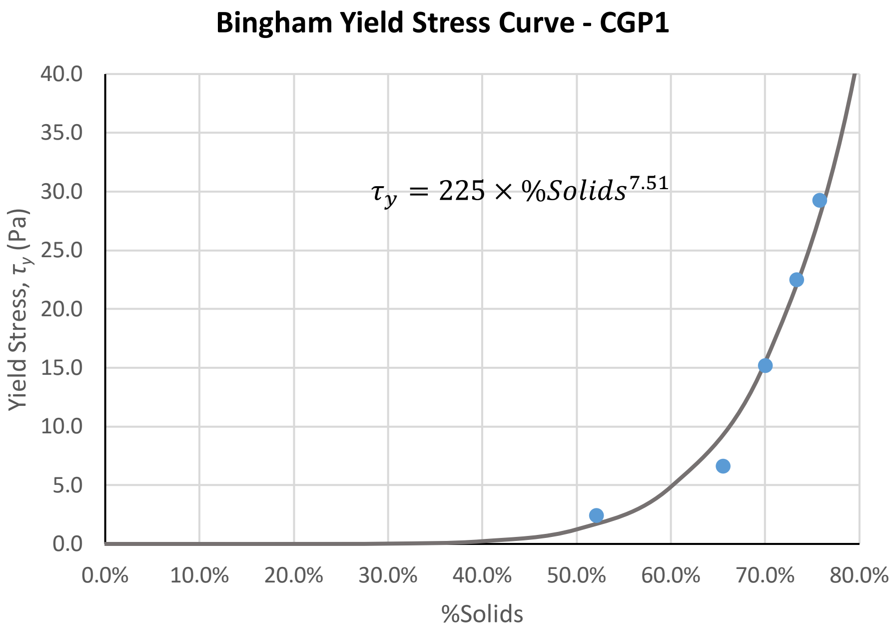


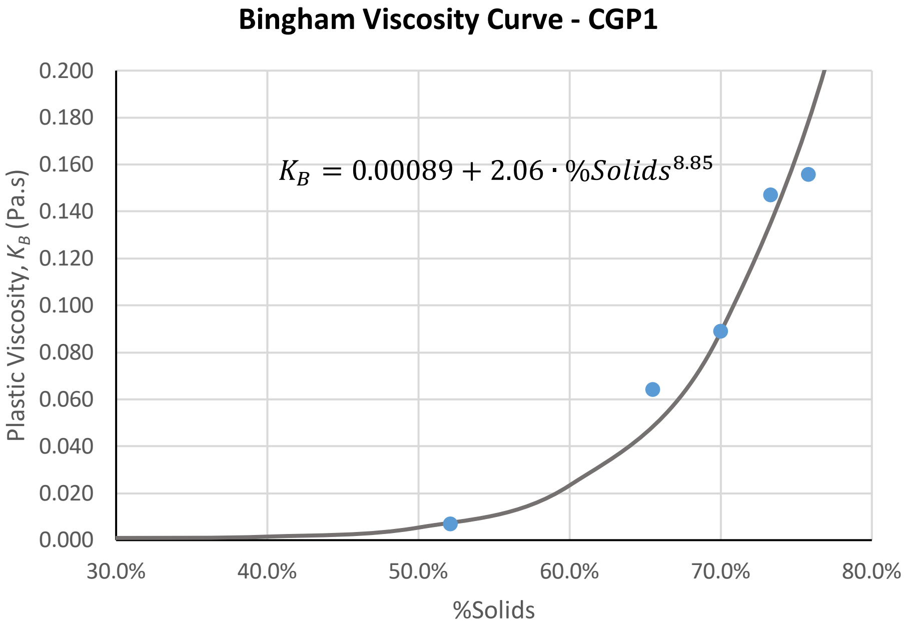
Table 5: Bingham Model Outputs – CGP1

%Solids	Yield Stress (Pa)	Plastic Viscosity (cP)
75.8%	29.3	155.9
73.3%	22.5	147.2
70.0%	15.2	89.0
65.5%	6.6	64.3
52.1%	2.4	7.0
34.6%	N.D	N.D

Graph 7: Bingham Yield Stress Curve - CGP1



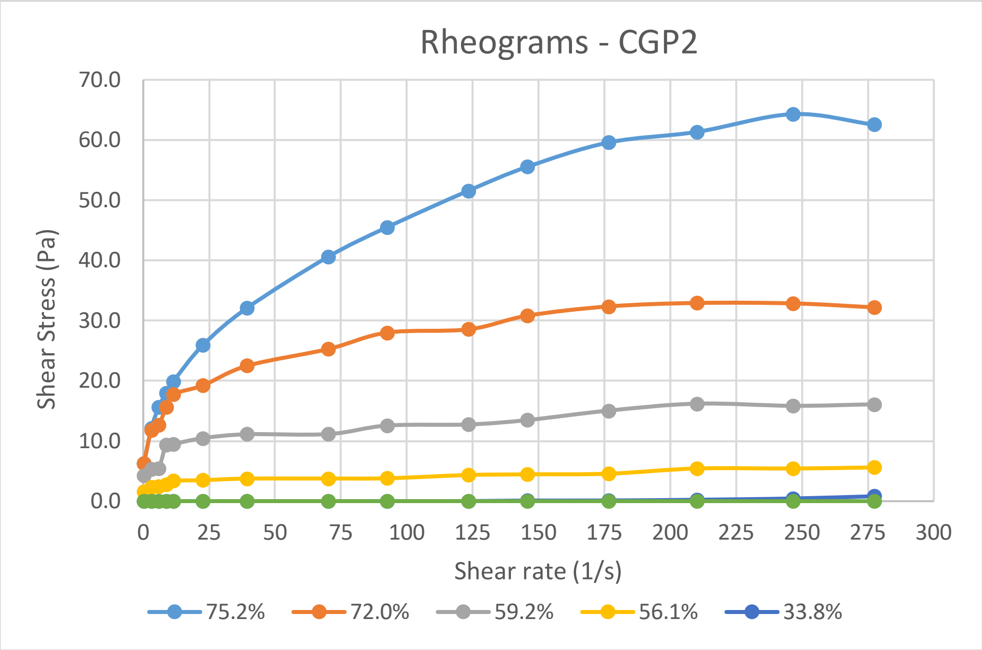
Graph 8: Bingham Viscosity Curve - CGP1



At the as-received 34.6% solids, CGP1 behaved as a very fluid slurry, with low stresses and no measurable Bingham yield stress. Once concentrated, the material progressively thickened as yield stress increased from about 2 Pa at ~52% solids to ~15–30 Pa at 70–75.8% solids. Plastic viscosity followed the same pattern, rising from ~7 cP at ~52% solids to up to ~150 cP at 75.8%.

4.2 CGP2

Graph 9: Rheograms – CGP2



Graph 10: Viscosity Curves – CGP2

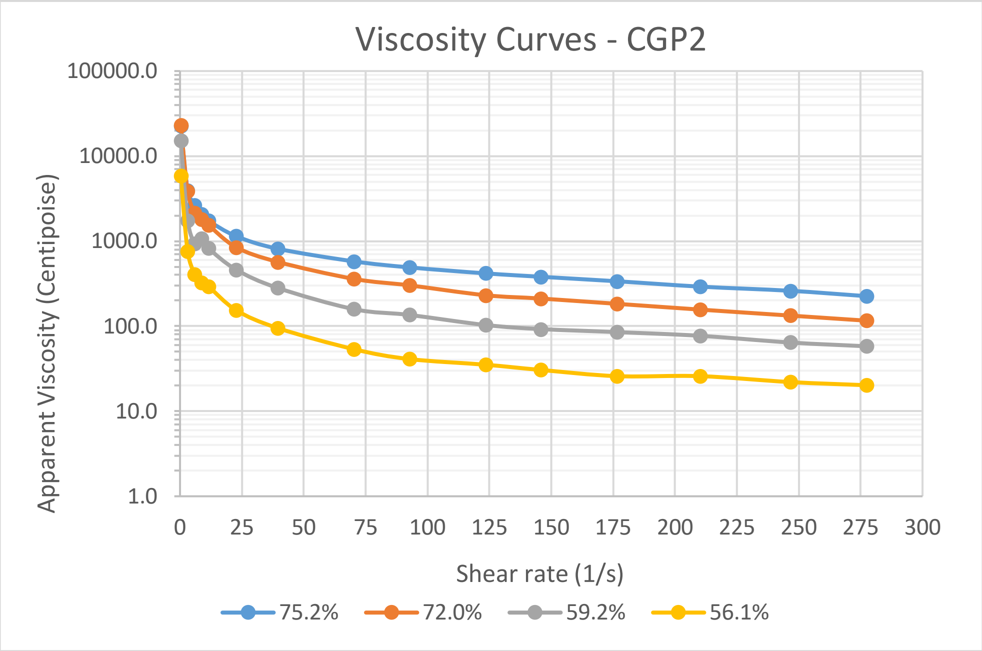
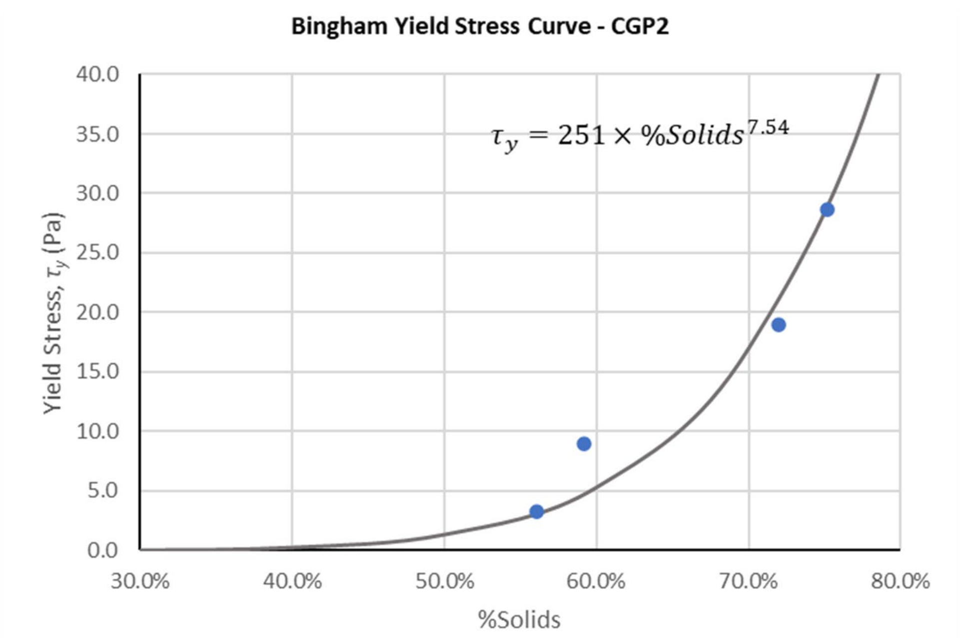


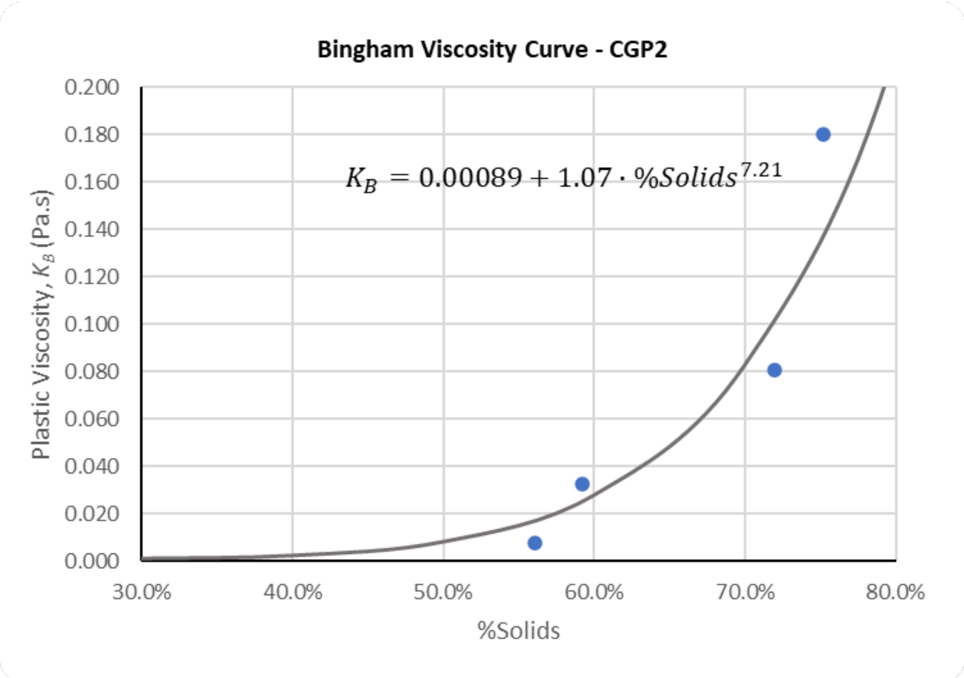
Table 6: Bingham Model Outputs – CGP2

%Solids	Yield Stress (Pa)	Plastic Viscosity (cP)
75.2%	28.66	180.0
72.0%	18.95	80.6
59.2%	9.02	32.7
56.1%	3.31	7.6
33.8%	N.D	N.D

Graph 11: Bingham Yield Stress Curve – CGP2



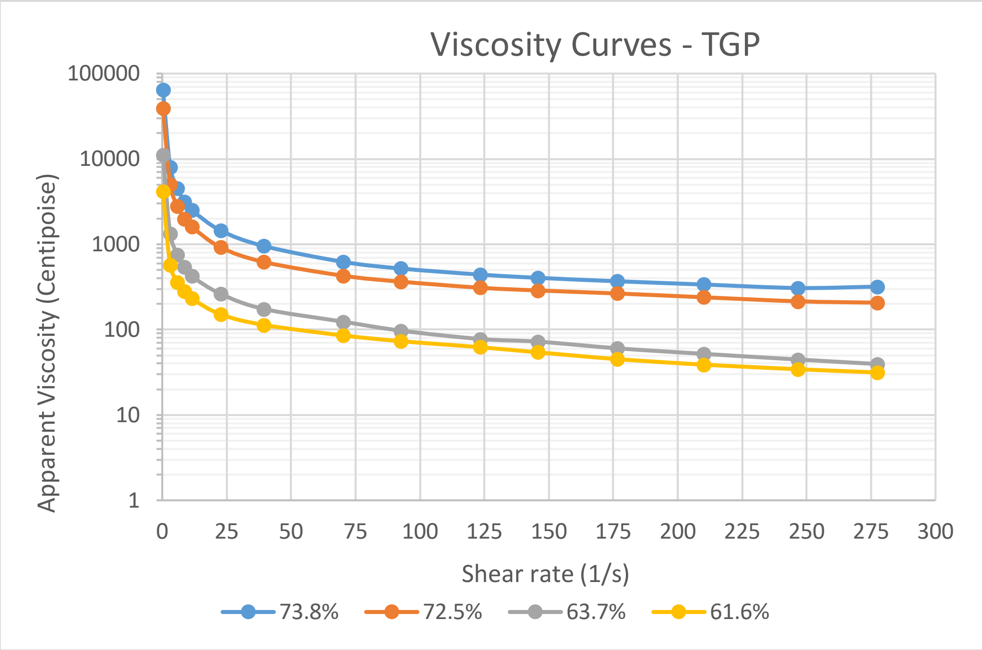
Graph 12: Bingham Viscosity Curve – CGP2



Similarly to the CGP1 tails, for CGP2, the as-received 33.8% solids slurry showed very low resistance to flow, with no clear yield stress and plastic viscosity in the order of 1 cP. Yield stress then climbed from ~3–9 Pa at ~56–59% solids ~29 Pa at 75.2%. Plastic viscosity rose from ~8 cP at ~56% solids to ~80–180 cP at 72–75.2%.

4.3 TGP

Graph 13: Viscosity Curves - TGP



Graph 14: Rheograms – TGP

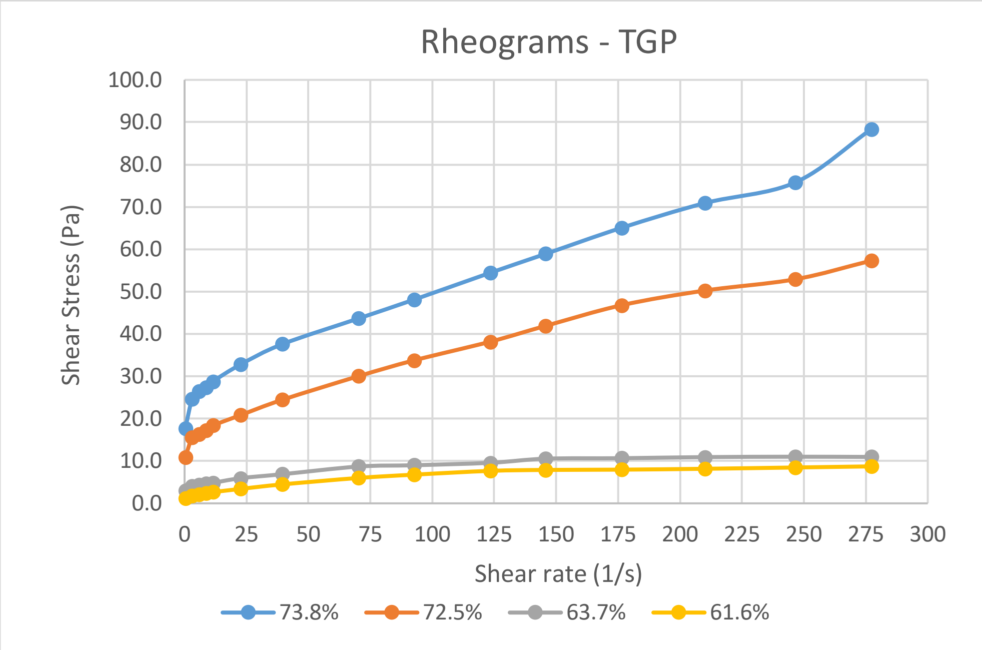


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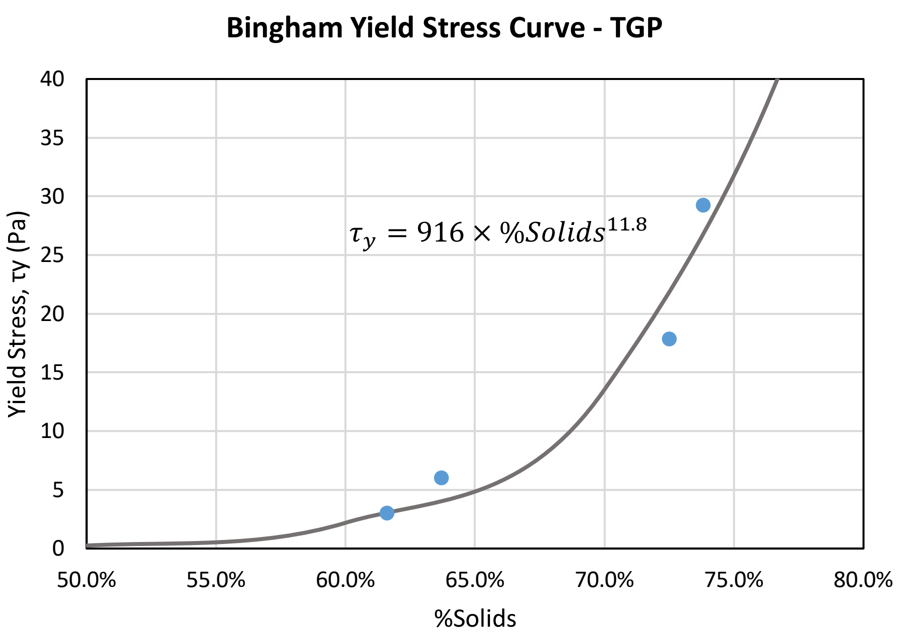
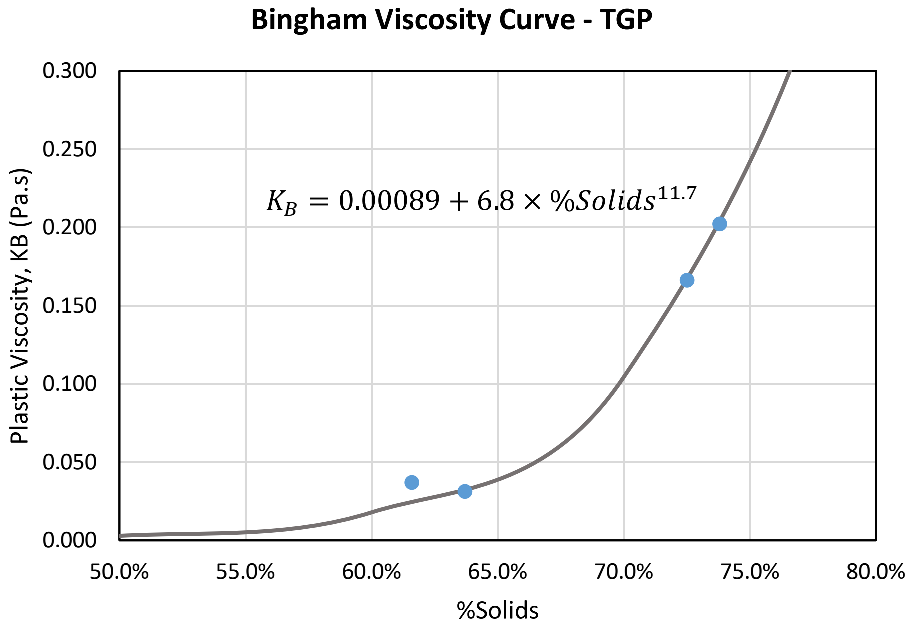
Table 7: Bingham Model Outputs – TGP

%Solids	Yield Stress (Pa)	Plastic Viscosity (cP)
73.8%	29.21	202
72.5%	17.81	166
63.7%	6.01	31
61.6%	3.02	37
3.8%	N.D	N.D

Graph 15: Bingham Yield Stress Curve – TGP



Graph 16: Bingham Viscosity Curve – TGP



At the received concentration of 3.8% solids, TGP tailings had very low shear stresses and no measurable yield stress. At higher solids concentrations, yield stressed increased from ~3 Pa at 61.6% solids to 29 Pa at 73.8%. Plastic viscosity follows the same trend, rising from ~31–37 cP at ~62–64% solids to ~166–202 cP at 72.5–73.8%.

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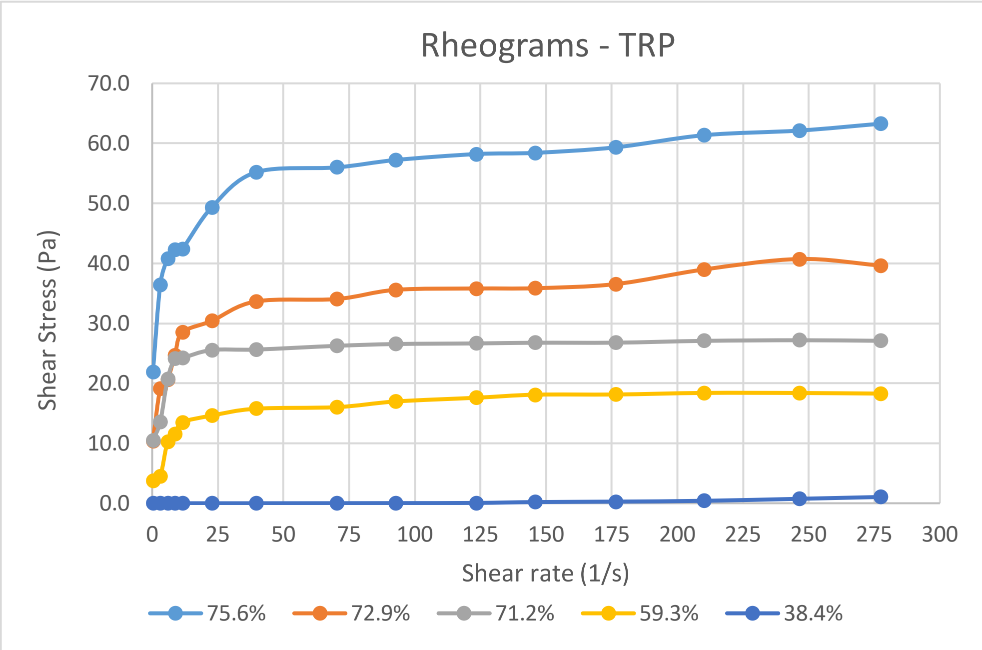
4.4 TRP

Graph 17: Rheograms – TRP



Graph 18: Viscosity Curves - TRP

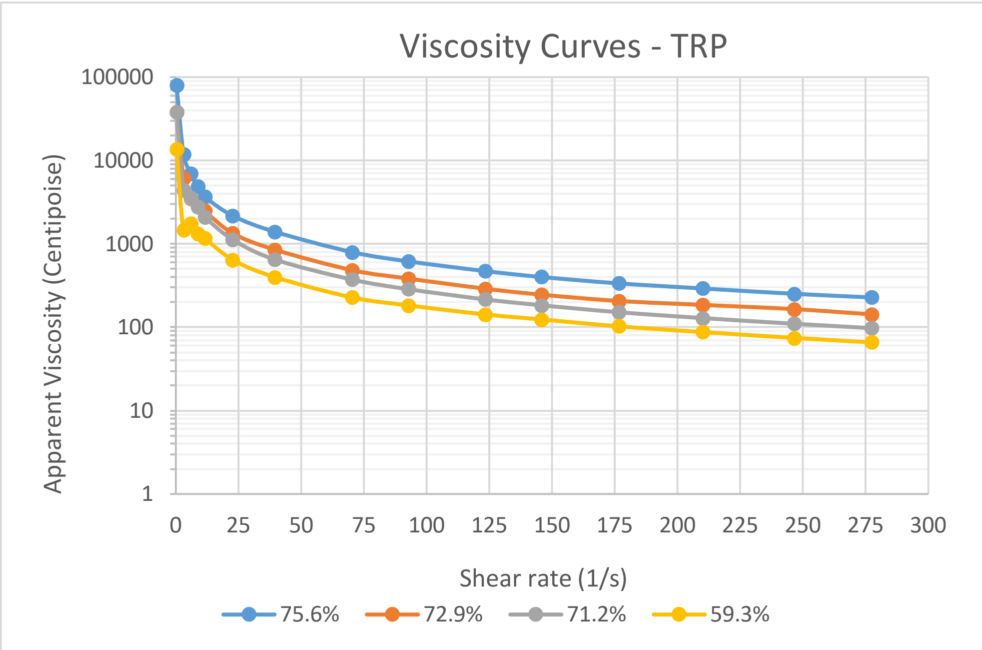


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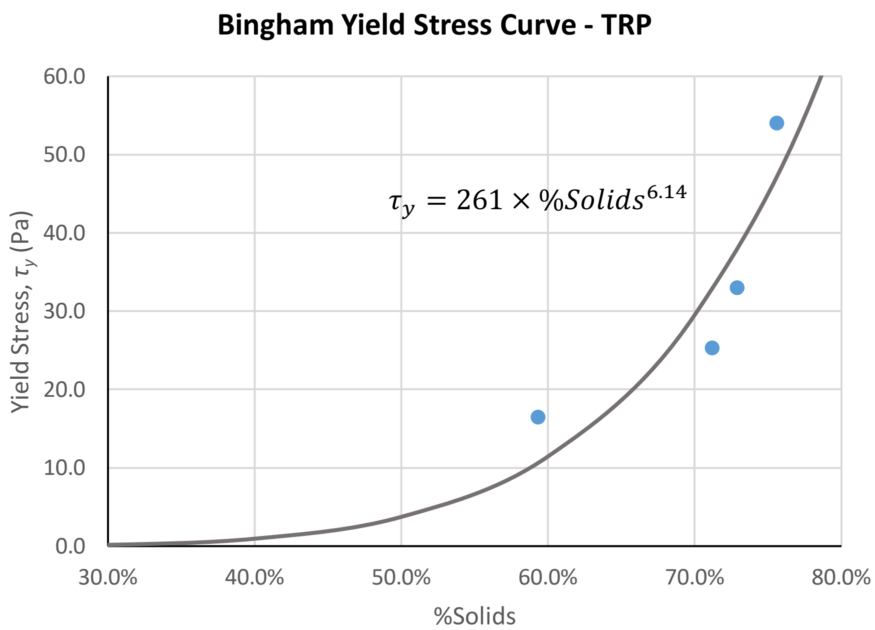
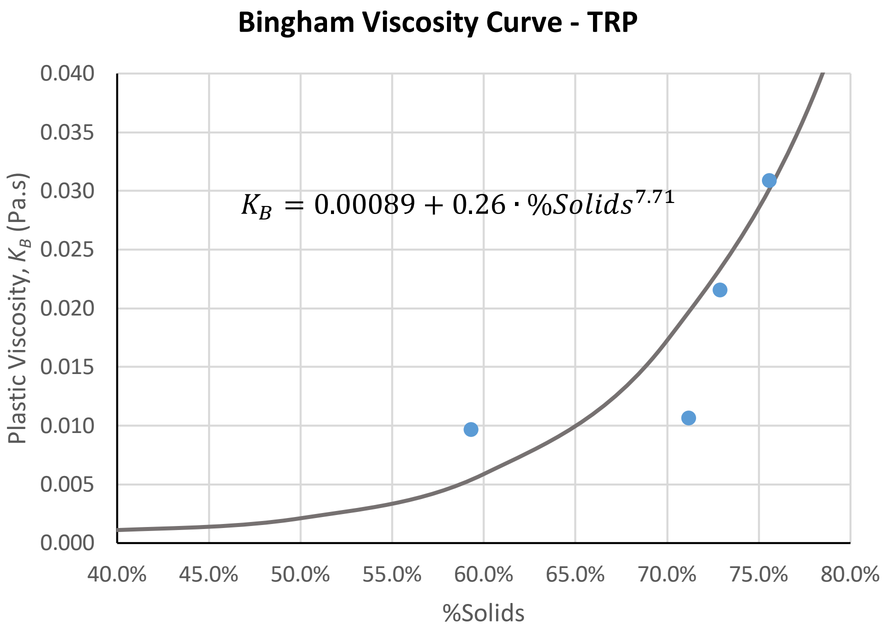
Table 8: Bingham Model Outputs – TRP

%Solids	Yield Stress (Pa)	Plastic Viscosity (cP)
75.6%	54.06	30.9
72.9%	32.99	21.6
71.2%	25.35	10.6
59.3%	16.50	9.7
38.4%	N.D	N.D

Graph 19: Bingham Yield Stress Curve – TRP



Graph 20: Bingham Viscosity Curve – TRP



At 38.4% solids the TRP tailings, stresses and viscosities are low and no yield stress could be reliably fitted. As solids increase, yield stress rises from ~16 Pa at 59.3% solids to ~54 Pa at 75.6%. Plastic viscosity increases from ~10 cP at ~59–71% solids to ~22–31 cP at 72.9–75.6%.

5 Conclusion

Fremantle Metallurgy has completed particle size distribution and rheology testwork on the CGP1, CGP2, TGP and TRP tailings streams from Talison Lithium's Greenbushes operation. Sieve analyses show that all four streams are relatively coarse, with P80 values in the range of 190 -225 µm and P50 values around 110 - 130 µm. CGP1 and TRP plot towards the finer end of this range, while CGP2 and TGP are slightly coarser, with a larger proportion of material retained in the 75 - 212 µm size classes.

At the as-received solids contents (34.6% CGP1, 33.8% CGP2, 42.2% TRP and 3.8% TGP), all four slurries behaved as relatively fluid suspensions, with low shear stresses and apparent viscosities and no determinable Bingham yield stress.

To better characterise behaviour under more demanding conditions, each stream was therefore tested at much higher solids concentrations. For all samples, yield stresses at high solids are broadly similar, reaching approximately 25 to 30 Pa at 72 to 76% w/w solids, with plastic viscosities in the range of 150 - 200 cP at these conditions. The exception was the TRP tailings which yielded at 54Pa at similar solids densities.

The rheological behaviour of the samples may be cause by the relatively coarse, sandy nature of the particles. Even at elevated solids, apparent viscosities at pumping-relevant shear rates remain reasonable once the material has begun to flow, despite very high apparent viscosities at low shear for the higher solids tests. In practice, care should be taken when designing the pumping system such that sanding does not occur.

6 Glossary

- **Yield Stress (Pa)**
  The minimum stress required to initiate flow in a slurry. Below this point, the material behaves like a solid; above it, the slurry begins to move.
- **Plastic Viscosity (cP)**
  A measure of the resistance to flow once movement has started, represented by the slope of the shear stress vs shear rate curve in the Bingham Plastic model.
- **Apparent Viscosity (cP)**
  The effective viscosity of the slurry at a given shear rate. It varies with agitation and shear conditions.
- **Shear Rate (s^{-1})**
  The rate at which adjacent layers of slurry move relative to each other. Low shear corresponds to gentle movement (as in slow stirring), while high shear occurs under strong agitation or pumping.

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7 Appendix

7.1 CGP1

Table 9: Rheology Data (Shear Stress) - CGP1

%Solids	Shear Stress [Pa] at Specific Shear Rate [1/s]														
	277.3	246.5	210.1	176.5	145.8	123.4	92.6	70.2	39.4	22.7	11.5	8.7	5.9	3.1	0.3
75.8%	94.1	75.2	63.9	56.3	49.9	47.4	43.9	41.8	33.0	27.7	24.6	24.0	23.1	22.4	16.6
73.3%	56.2	51.2	48.7	46.1	43.1	40.7	36.9	33.6	28.6	24.8	21.8	21.0	20.4	19.4	15.2
70.0%	26.0	27.7	28.3	28.2	27.3	26.2	24.1	22.2	18.9	16.2	14.0	13.5	13.0	12.2	9.7
65.5%	10.8	12.3	12.9	13.3	13.4	13.0	12.3	11.4	9.4	8.1	7.1	6.7	6.3	6.0	4.4
52.1%	4.6	5.5	4.6	3.9	3.3	3.2	3.0	2.9	2.8	2.6	2.2	2.1	2.2	2.1	1.4
34.0%	1.6	1.0	0.7	0.6	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Table 10: Rheology Data (Apparent Viscosity) - CGP1

%Solids	Apparent Viscosity [Centipoise] at Specific Shear Rate [1/s]														
	277.3	246.5	210.1	176.5	145.8	123.4	92.6	70.2	39.4	22.7	11.5	8.7	5.9	3.1	0.3
75.8%	339	305	304	319	342	384	474	595	837	1224	2143	2774	3930	7281	59199
73.3%	203	208	232	261	296	330	398	478	724	1094	1902	2424	3468	6303	54404
70.0%	94	112	135	159	188	213	260	316	479	715	1222	1553	2219	3984	34604
65.5%	39	50	61	75	92	106	133	162	239	360	616	768	1074	1945	15771
52.1%	17	22	22	22	22	26	33	42	70	115	192	248	372	671	5028
34.0%	6	4	3	4	3	2	0	0	0	0	0	0	0	0	0

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Table 11: Rheology Data (Torque) – CGP1

%Solids	Torque [µN.m] at Specific Shear Rate [1/s]														
	277.3	**246.5**	**210.1**	**176.5**	**145.8**	**123.4**	**92.6**	**70.2**	**39.4**	**22.7**	**11.5**	**8.7**	**5.9**	**3.1**	**0.3**
75.8%	11117	8877	7549	6649	5888	5597	5186	4937	3902	3277	2903	2840	2725	2642	1955
73.3%	6634	6045	5755	5448	5094	4807	4355	3963	3374	2927	2576	2482	2405	2287	1797
70.0%	3070	3272	3344	3325	3228	3098	2845	2618	2232	1913	1655	1590	1539	1446	1143
65.5%	1273	1453	1518	1567	1579	1541	1454	1342	1115	962	834	786	745	706	521
52.1%	547	646	541	456	386	376	358	345	328	306	260	254	258	243	166
34.0%	186	120	86	73	59	35	3	0	0	0	0	0	0	0	0

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7.2 CGP2

Table 12: Rheology Data (Shear Stress) – CGP2

%Solids	Shear Stress [Pa] at Specific Shear Rate [1/s]													
	277.3	246.5	210.1	176.5	145.8	123.4	92.6	70.2	39.4	22.7	11.5	8.7	5.9	3.1	0.3
75.2%	62.55	64.30	61.34	59.59	55.54	51.57	45.52	40.61	32.11	25.93	19.93	17.97	15.64	12.08	6.30
72.0%	32.20	32.86	32.93	32.35	30.82	28.54	28.01	25.28	22.49	19.23	17.77	15.59	12.66	11.82	6.32
59.2%	16.10	15.84	16.20	15.05	13.48	12.75	12.57	11.14	11.12	10.47	9.50	9.34	5.47	5.36	4.22
56.1%	5.61	5.43	5.43	4.56	4.46	4.35	3.80	3.77	3.75	3.49	3.38	2.82	2.41	2.33	1.62
33.8%	0.81	0.45	0.24	0.12	0.10	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Table 13: Rheology Data (Apparent Viscosity) – CGP2

%Solids	Apparent Viscosity [Centipoise] at Specific Shear Rate [1/s]													
	277.3	246.5	210.1	176.5	145.8	123.4	92.6	70.2	39.4	22.7	11.5	8.7	5.9	3.1	0.3
75.2%	225.6	260.8	291.9	337.5	381.0	418.0	491.5	578.3	814.0	1144.3	1737.6	2073.3	2663.7	3929.1	22818.8
72.0%	116.1	133.3	156.7	183.2	211.4	231.3	302.4	359.9	570.2	848.6	1549.2	1798.4	2155.5	3843.7	22899.1
59.2%	58.1	64.3	77.1	85.2	92.5	103.3	135.7	158.7	281.8	462.3	828.1	1077.5	931.0	1744.9	15272.9
56.1%	20.2	22.0	25.9	25.8	30.6	35.2	41.1	53.7	95.1	154.2	294.4	325.8	410.1	759.3	5851.0
33.8%	2.9	1.8	1.1	0.7	0.7	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

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Table 14: Rheology Data (Torque) – CGP2

%Solids	Torque [µN.m] at Specific Shear Rate [1/s]														
	277.3	**246.5**	**210.1**	**176.5**	**145.8**	**123.4**	**92.6**	**70.2**	**39.4**	**22.7**	**11.5**	**8.7**	**5.9**	**3.1**	**0.3**
75.2%	7387.1	7593.5	7244.9	7037.2	6560.0	6090.8	5376.2	4796.4	3792.3	3062.3	2353.5	2122.9	1847.1	1426.5	744.3
72.0%	3802.9	3880.5	3889.0	3820.7	3639.7	3371.1	3307.8	2985.2	2656.6	2271.0	2098.4	1841.3	1494.7	1395.5	746.9
59.2%	1901.0	1871.1	1913.5	1777.1	1591.6	1505.2	1484.2	1315.9	1313.0	1237.1	1121.7	1103.2	645.6	633.5	498.2
56.1%	662.2	641.3	641.7	539.0	526.7	513.4	449.3	445.1	443.0	412.8	398.8	333.6	284.4	275.7	190.9
33.8%	96.1	52.8	27.8	13.8	12.0	1.8	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

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7.3 TGP

Table 15: Rheology Data (Shear Stress) - TGP

%Solids	Shear Stress [Pa] at Specific Shear Rate [1/s]														
	277.3	**246.5**	**210.1**	**176.5**	**145.8**	**123.4**	**92.6**	**70.2**	**39.4**	**22.7**	**11.5**	**8.7**	**5.9**	**3.1**	**0.3**
73.8%	88.40	75.78	70.92	65.09	58.91	54.44	48.10	43.66	37.59	32.81	28.81	27.36	26.47	24.62	17.70
72.5%	57.32	52.91	50.26	46.80	41.91	38.17	33.76	30.03	24.45	20.84	18.39	17.26	16.26	15.52	10.88
63.7%	10.96	11.01	10.92	10.66	10.54	9.58	9.00	8.69	6.88	5.95	4.84	4.67	4.44	4.07	3.04
61.6%	8.73	8.47	8.17	7.96	7.89	7.67	6.78	6.00	4.48	3.42	2.65	2.45	2.12	1.75	1.14
3.8%	0.55	0.41	0.34	0.20	0.09	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Table 16: Rheology Data (Apparent Viscosity) - TGP

%Solids	Apparent Viscosity [Centipoise] at Specific Shear Rate [1/s]														
	277.3	**246.5**	**210.1**	**176.5**	**145.8**	**123.4**	**92.6**	**70.2**	**39.4**	**22.7**	**11.5**	**8.7**	**5.9**	**3.1**	**0.3**
73.8%	319	307	338	369	404	441	519	622	953	1448	2512	3156	4509	8009	64077
72.5%	207	215	239	265	288	309	365	428	620	920	1603	1991	2770	5049	39405
63.7%	40	45	52	60	72	78	97	124	174	262	422	539	756	1325	11014
61.6%	32	34	39	45	54	62	73	85	113	151	231	282	360	570	4133
3.8%	2	2	2	1	1	0	0	0	0	0	0	0	0	0	0

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Table 17: Rheology Data (Torque) – TGP

%Solids	Torque [μN.m] at Specific Shear Rate [1/s]														
	277.3	**246.5**	**210.1**	**176.5**	**145.8**	**123.4**	**92.6**	**70.2**	**39.4**	**22.7**	**11.5**	**8.7**	**5.9**	**3.1**	**0.3**
73.8%	10440	8950	8376	7687	6958	6430	5681	5156	4439	3875	3402	3231	3127	2908	2090
72.5%	6769	6249	5936	5527	4950	4508	3987	3547	2888	2462	2171	2038	1921	1833	1285
63.7%	1295	1301	1290	1259	1245	1131	1063	1027	813	702	572	552	524	481	359
61.6%	1032	1000	964	940	932	906	800	708	529	404	313	289	250	207	135
3.8%	65	49	40	24	11	0	0	0	0	0	0	0	0	0	0

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7.4 TRP

Table 18: Rheology Data (Shear Stress) - TRP

%Solids	Shear Stress [Pa] at Specific Shear Rate [1/s]														
	277.3	246.5	210.1	176.6	145.8	123.4	92.6	70.2	39.5	22.7	11.5	8.7	5.9	3.1	0.3
75.6%	63.3	62.1	61.4	59.3	58.4	58.2	57.2	56.0	55.2	49.3	42.4	42.3	40.8	36.4	21.9
72.9%	39.6	40.7	39.0	36.5	35.8	35.8	35.6	34.0	33.6	30.4	28.5	24.7	20.6	19.1	10.4
71.2%	27.1	27.2	27.1	26.8	26.8	26.6	26.5	26.2	25.6	25.5	24.2	24.1	20.7	13.6	10.5
59.3%	18.3	18.4	18.4	18.1	18.1	17.6	17.0	16.0	15.8	14.6	13.5	11.5	10.2	4.5	3.8
38.4%	1.0	0.7	0.4	0.3	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Table 19: Rheology Data (Apparent Viscosity) - TRP

%Solids	Apparent Viscosity [Centipoise] at Specific Shear Rate [1/s]														
	277.3	246.5	210.1	176.6	145.8	123.4	92.6	70.2	39.5	22.7	11.5	8.7	5.9	3.1	0.3
75.6%	228	252	292	336	401	472	618	797	1398	2177	3699	4881	6948	11865	79826
72.9%	143	165	185	207	246	290	384	485	853	1341	2482	2849	3518	6216	38018
71.2%	98	110	129	152	184	216	287	374	649	1127	2113	2781	3533	4420	38182
59.3%	66	75	88	103	124	143	183	228	399	645	1175	1327	1744	1460	13729
38.4%	4	3	2	2	1	0	0	0	0	0	0	0	0	0	0

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Table 20: Rheology Data (Torque) – TRP

%Solids	Torque [µN.m] at Specific Shear Rate [1/s]														
	277.3	**246.5**	**210.1**	**176.6**	**145.8**	**123.4**	**92.6**	**70.2**	**39.5**	**22.7**	**11.5**	**8.7**	**5.9**	**3.1**	**0.3**
75.6%	7472	7338	7246	7008	6899	6875	6757	6612	6516	5826	5009	4993	4815	4304	2583
72.9%	4681	4809	4602	4315	4234	4228	4201	4020	3973	3590	3361	2914	2438	2255	1230
71.2%	3198	3210	3197	3161	3160	3147	3135	3099	3026	3017	2861	2845	2448	1604	1236
59.3%	2159	2171	2172	2141	2137	2077	2003	1892	1861	1726	1591	1357	1209	530	444
38.4%	123	88	48	32	23	6	3	1	0	0	0	0	0	0	0